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# INVESTIGATION FOR DETERMINING THE TORQUE-TENSION RELATIONSHIP OF SCREW THREADED FASTENERS USED ON AIRCRAFT

ABRAHAM B. ASCH

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**JULY 1957** 

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# INVESTIGATION FOR DETERMINING THE TORQUE-TENSION RELATIONSHIP OF SCREW THREADED FASTENERS USED ON AIRCRAFT

ABRAHAM B. ASCH

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JULY 1957

SPECIAL PROJECTS BRANCH
AIRCRAFT LABORATORY
CONTRACT NO. AF 33 (616)-2808
PROJECT NO. 1318
TASK NO. 13444

WRIGHT AIR DEVELOPMENT CENTER
AIR RESEARCH AND DEVELOPMENT COMMAND
UNITED STATES AIR FORCE
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

### FOREWORD

This report, which describes the Torque-Tension Relationships of Screw Thread Fasteners for Aircraft, and the methods used to obtain these relationships, was prepared by Asch Equipment Company of Dayton, Ohio, Order No. P-1227.

This program was performed under Contract No. AF 33(616)-2808, Project No. 1318, Task No. 13444, for the Special Projects Branch WCLSJ-3 of the Aircraft Laboratory, Wright Air Development Center, Mr. A. B. Nutt, Branch Chief, Mr. J. W. Evans, Section Chief and Mr. F. A. Hannon, Project Engineer.

Work on this project was begun on January 28, 1955 and was completed June 21, 1957.

## ABSTRACT

This report describes the work done and the results obtained during a program to determine the relationship between the torque required to tighten various types of aircraft bolts and screws and the tensile stress induced in the root area of these bolts and screws by this torque.

The torque-tension relationship was investigated for successive tightenings to high tensile stress levels from the head and nut, with and without lubrication.

The bolts upon which tests were performed were the MS-20,004 to MS-20,024 series (14 sizes), the AN-3C to AN-2OC series (13 sizes), and the AN-509-CR to AN-509-916R series flat head screws (8 sizes).

For conditions of dry torquing the torque-tension relationship was found to be a function of many variables; among which were:

- 1. The type of metal, hardness and surface finish of the plates being bolted.
- 2. The amount of clearance in the hole drilled to accommodate the bolt.
- 3. The type of metal, hardness and plated or unplated condition of the bolts and nuts.
- 4. The geometry and surface finish of the head and nut bearing surfaces.
- 5. The number of successive tightenings.

Lubricated condition torquing produces average torque-tension relationships which do not vary appreciably over repeated torquings to the high tensile stress levels.

The above listed variables do not play as important a role in the case of lubricated torquing.

The increase in torque value for the dry condition for successive tightenings to the same stress level is due principally to two factors:

- 1. Galling of the head or nut seating surfaces.
- 2. Galling of the threads between the nut and bolt.

Preliminary tests indicate that #1 accounts for a considerably greater percentage of the increase in torque values than does thread galling, which suggests a method of partially lubricated torquing.

### PUBLICATION REVIEW

The publication of this report does not constitute approval by the Air Force of the findings or conclusions herein. It is published only for the exchange and stimulation of ideas.

FOR THE COMMANDER:

Colonel WAT

Chief, Aircraft Laboratory

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## SECTION I

## INTRODUCTION

**PURPOSE** 

The purpose of this contract is to determine the relationship between torque required to tighten various types of aircraft bolts and screws, and the tensile stress induced in the root area of these bolts and screws by this torque.

TEST CONDITIONS The relationship was investigated for repeated torquings from the head, and from the nut, with and without lubrication. Hardness and surface finish tests were also made for comparison purposes.

BOLTS TESTED All sizes in the MS-20,004 to MS-20,024 series, the AN-509-8R to AN-509-916R series and the AN-3C to AN-2OC series were tested with suitable nuts. All nuts and bolts used were purchased in the open market with the exception of a limited number of nuts furnished by two aircraft manufacturers for comparison purposes.

TEST EQUIPMENT The tests were performed on a special testing machine designed and built for the purpose, and capable of producing indications of torque and tension simultaneously.

Manuscript released by the author June, 1957 for publication as a WADC Technical Report.

## SECTION II

## SPECIMENS

BOLTS
TESTED

Tests were performed on the following bolts and nuts:

	the state of the s	
Sizes	Bolt	Nut
1)1	MS-20,004 to MS-20,024	EB
6	MS-20,009 to MS-20,018	42 FW
8	AN-509-8R to AN-509-916R	AN-365
3	AN-509-8R to AN-509-416R	NMJ
9	AN-3C to AN-12C	AN-363-0
4	AN-14C to AN-20C	AN-310-C

Tables 1, 2 and 3, lists the sizes tested and the coded designations.

## SPECIMEN IDENTIFI - CATION

The specimens used for the torque tension tests were identified by a code comprised of letters and digits indicating the following:

The first letter or letters designate the size of the bolt and the type as noted in Tables 1, 2 and 3.

The second digit indicates the specimen number. Five specimens were used for each condition of test.

The third letter is either H or N indicating whether the specimen was torqued from the head or from the nut.

When lubrication was used in testing the specimen, a fourth letter L was added to the code designation.

For example, the specimen E-3-N-L is the third specimen of the MS-20,008 bolt group and was torqued from the nut after the application of lubricant to the threads and to both the nut and head seating surfaces.

During the course of the test program, several sizes of nuts which were supplied by Lockheed Aircraft Corporation and by Boeing Airplane Company were tested. These nuts were used with bolts F, G, H, I, J and K in the MS-20,009 to MS-20,018 series. These have been further identified in the "Test Data" sheets by the letter A for the nuts supplied by Lockheed and the letter B for the nuts supplied by Boeing. This letter appears before the specimen number.

Appendix I contains the dimensional details of the bolts and nuts used. Figure 1. shows the various types of specimens used.

(3-EACH USED ON BOLS-F, 6, H, E, L,
SIDNOVED ERESSED SLEET - USEM HICH LENSITE EXLEGNAT MEHNCHING
EXLEGNOF MENCHING NOLS
AUTS - ELASTIC STOP NUT CORP - TYPE EB COUBLE HEX. HIGH TENSILE
SINAWWOD

			124	Y 30 V V V V
ZDZ-83	21291	1/2-12 UNE-3A	ZS-DZ00Z·SW	<b>N</b>
222-83	20921	48-7NU ZI-8/21	Z9-ZZ00Z-SW	W
Z0Z-83	TE10.1	48-7NU 21-5/1	09-0200Z-SW	7
Z181-M1Zb Z81-83	81180	AE-7NU Z1-8/1	09-8100Z-SW	K
t191-M12t t>91-83	かりかりつ	AE- 7NU P/-1	09-9100Z-SW	Γ
DIDI-MIZT DDI-83	90810	AE-7NU A1-8/	05-0100Z-SW	I
9121M12b	8198.0	AE-7NU 01-D/E	09-2100Z-SW	H
8101-MJZ# 801-82	00020	AE-7NU 81-8/2	09-0100Z-SW	9
816-M32t 860-83	8881.0	9/c-18 UNE-3A	09-6000Z-SW	1
080-83	98110	12-20 UNE-3A	09-8000Z-SW	3
0L0-83	06010	AE-3NU 05-01/	09-L000Z-SW	0
t90-83	6080.0	48-70 UNF-38	09-9000Z-SW	2
190-83	DZ90'0	HE-JNN DZ-9/5	09-9000Z-SW	8
840-83	9750.0	14-28 UNF-3A	Zt-+000Z-SW	H
ON LAN	A301 AREA SO IN.	azis ayaahl	AN STANDARD	-8N -3000

XIECD FOINT - 140,000 LESONIL

— 0315<u>31 s1708</u> sw —

AN 509 SERIES SCRE YIELD POINT - 130,000

000E N.e.	AN STANDARD Nº:	THREAD SIZE	18007 ,918EA SQ. 1W.	NUT NO.	ł
0	AN 509-8R37	8-32 NC-3A	0.0120	AU365-852	1
Q	AU 509-10837	10-32 NF-3A	0.0175	AN365-1032	1
8	AU509-216837	14-28 UNF-34	3.0326	AN 365-428	1 .
Q	AN 509-516 RAB	5/4-24 UNF-3A	0.0528	AN 365-524	4
Ŋ	AN509-616R48	38-24 UNF-34	0.0809	AN 365-624	ı
7	AN509-716R48	1/6-20UNF-3A	05010	AN 365-720	ľ
7	PN509-816R49	12-20UNF-3A	0.1436	AN 365-520	
>	AN509-916R52	911-18UNF-3H	0.1838	AN 365-918	
			-		1
					(
N	AN509-8R37	8-32 LIC-3A	0.0120	28-INN	
×	AN 509 - 10837	10-32 NF-3A	0.0175	NW5-02	
>	AU509-416237	14-28 UNF-3A	0.03260	NWJ-043	, ,
COMMENTS	TUPII V.	STEEL 11175 - 01/21/5			l
<b>10-0</b> 0	(5,101/)	19 (2)			

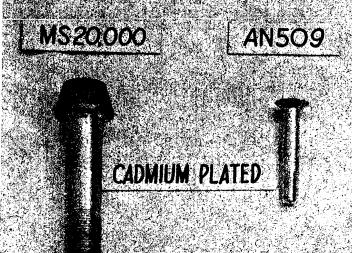
DOIENE	C1350 01-1/2 3108H	
32/5	21-t/60L- DETENIE - SLAN	_
		-

			· 51/1/30	NONO
				<u> </u>
CZ-DETETYET	LE201	48-2NNZ1-7/1	9p-202 NH	W-W
81-2018 NG	81180	48-7NU ZI-81	DD -281 NU	7-7
91-2018 NH	0.6464	HE- AN DI-1	ZD -791 NU	オ-ガ
PIDOIENE	90870	48- 7ND DI-8/2	ZD - 201 NU	7-1
DN 363C-1216	8198.0	4E-7ND 91-P/E	10-021 NU	I-I
8101-0838 NA	00000	UE-3N181-8/5	LE - 201 NH	H-H
816 - 2898 NU	88810	HE-HN181-91/6	LE - 26 NH	9-9
028-2818 NA .	98110	12-20 UNE-3A	LE-78 NH	4-4
02L - 2898 NH	06010	HE- 7N1 02-91/	98-71 NA	3-3
DZ9-2898NH	60800	AE-7NU DZ-86	98-79 NA	0.0
DZ9-2898NU	DZ90'0	48-74 UNF-3A	98 - 29 NH	2-2
874-289ENU	9780'0	4E-7NU 82-01	08-JDNA	8-8
7801-289ENU	SL10:0	HE-3N ZE-01	08-28 NA	<i>H-H</i>
5N LNN	ROOT AREA SO. IN.	azis adaahl	DARDNATZ NA	5N 2002

VIELD POINT - III,000 <sup>18</sup>/<sub>18</sub>/<sub>18</sub>/<sub>18</sub>

FIG. 1

## TYPES OF BOLTS TESTED







STAINLESS STEEL

## TYPES OF NUTS TESTED



42FW

AN365



AN363-C SILVER PLATED





EB

9

NMJ-363-C

ALUMINUM



AN 310-C
STAINLESS STEEL

TYPES OF BOLTS & NUTS TESTED

## SECTION III

## TESTS AND EQUIPMENT

TORQUE-TENSION TESTS In order to test the bolt torque-tension relationship, a special testing machine was designed and built. This testing machine incorporates a motorized drive for torquing the bolts. See Fig. 2.

Tension measurements were made by compressing calibrated strain gage load cells with the bolts. Four sizes of load cells were used for the complete range of bolt tension. Calibration of the compression cells was performed on a Tinius-Olsen Compression Tester, with a capacity of 200,000 lbs. Fig. 3 shows the compression cells.

Torsion measurements were made on calibrated torsion load cells. Four sizes were used for the complete range of torsion. Calibration of the torsion cells was performed on a Tinius-Olsen Torsion Tester, with a capacity of 60,000 in. lbs. Fig. 4 shows the torsion cells.

Bolt tension and torsion measurements were read directly from Asch Equipment Company self balancing type strain indicators. See Fig. 2.

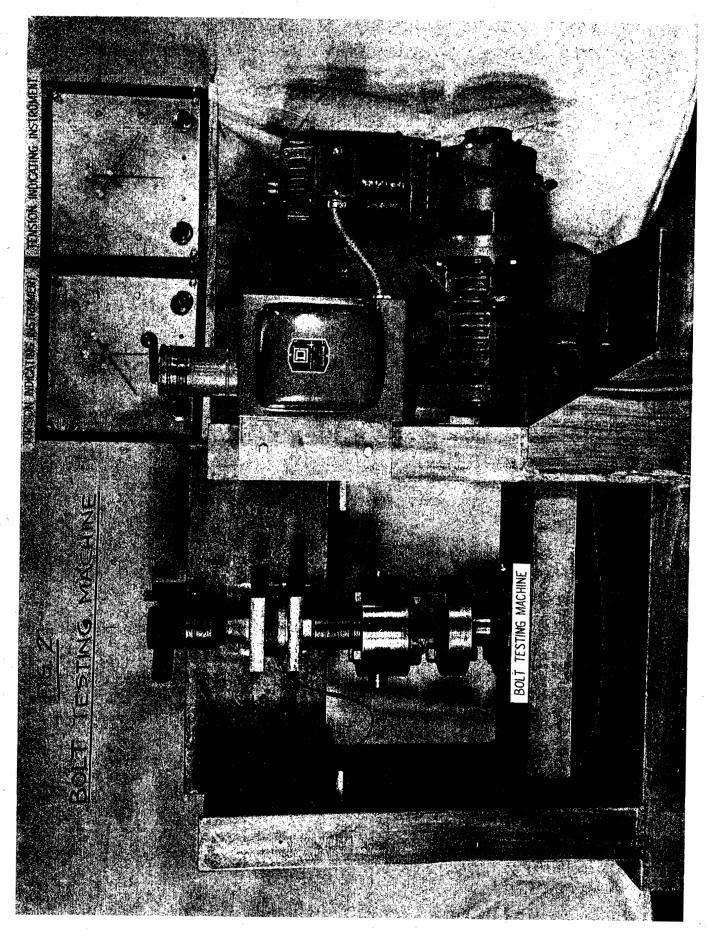
The test set up for the different types of bolts are shown in Fig. 5, 6 and 7.

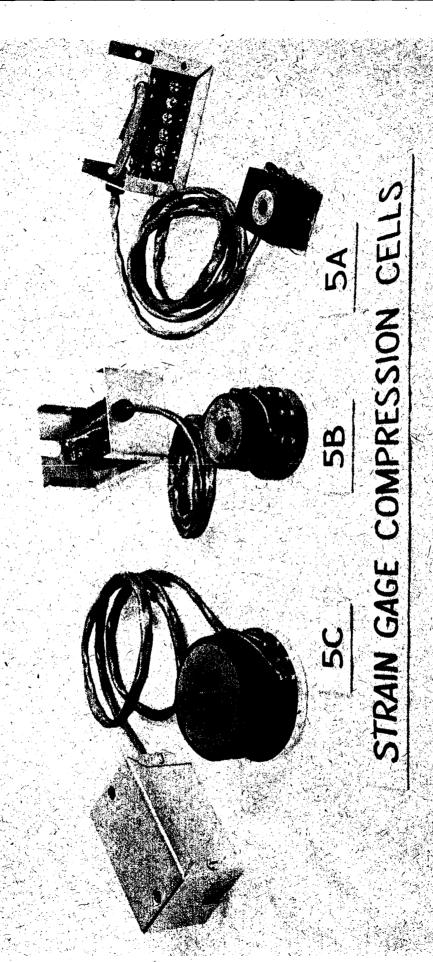
HARDNESS TESTS Hardness tests were made on several specimens from each type and for each size of the bolts and nuts, and also on representative spacer blocks. These were made on a Rockwell Hardness Tester.

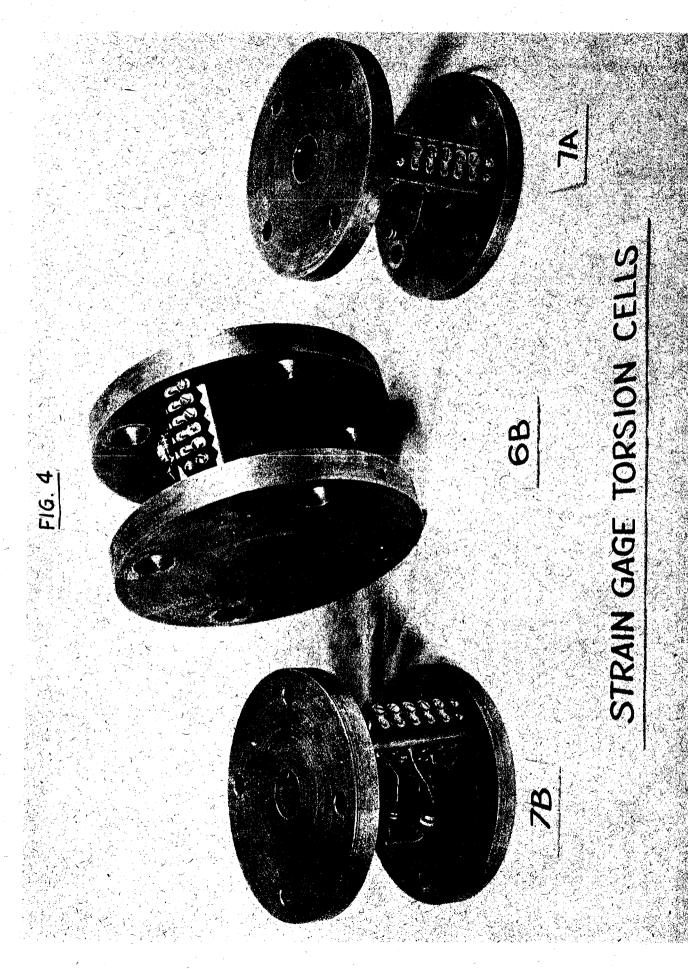
The spacer blocks were countersunk to allow clearance for the fillets under the heads of the MS-20,004 to MS-20,024 series bolts.

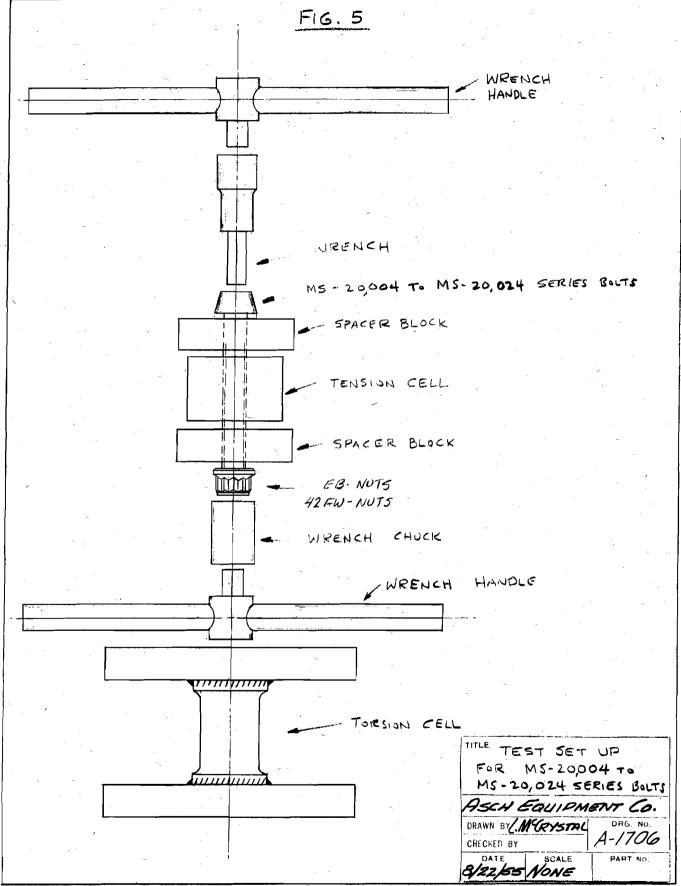
and the AN-3C to AN-2OC series bolts, and also-for the flat heads of the AN-509-8R to AN-509-916R series screws. Contours are shown on the "Test Data" sheets in Appendix III. The spacer blocks used with the nuts were not countersunk. Spacer blocks are shown in Fig. 8.

SURFACE FINISH TESTS Tests were also performed on the same specimens for finish of the seating surface of the heads and the nuts where they contact the spacer blocks, and also of the bearing surface of the spacer blocks. A Profilometer was used for these tests. Prior to making the tests, the Profilometer used was calibrated against known standards and found to be indicating 75% of the R.M.S. values. In the data sheets a correction factor of 1.33 was applied to the Profilometer readings.

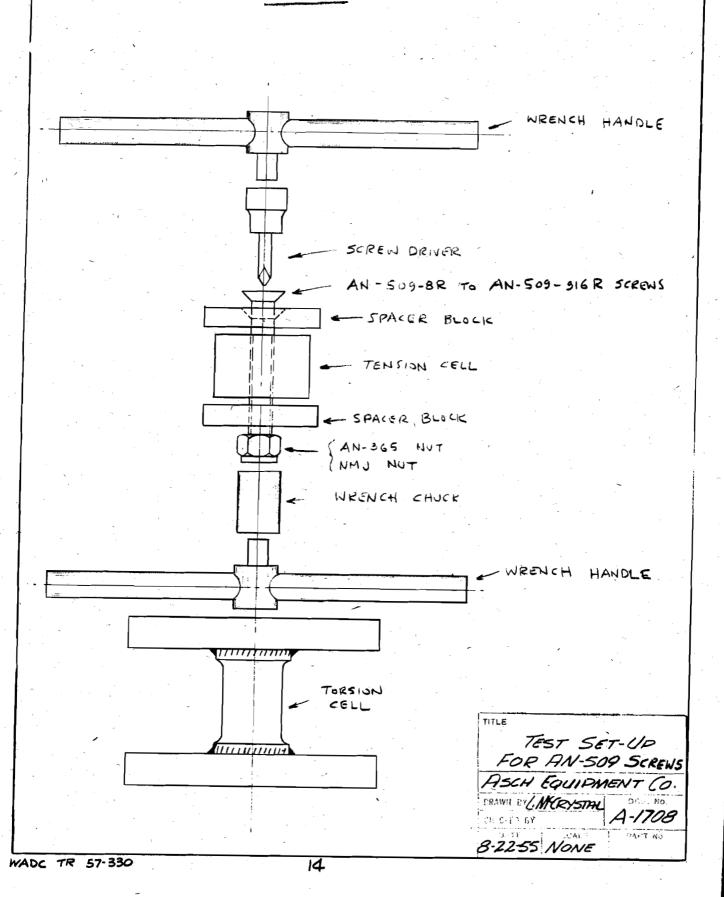


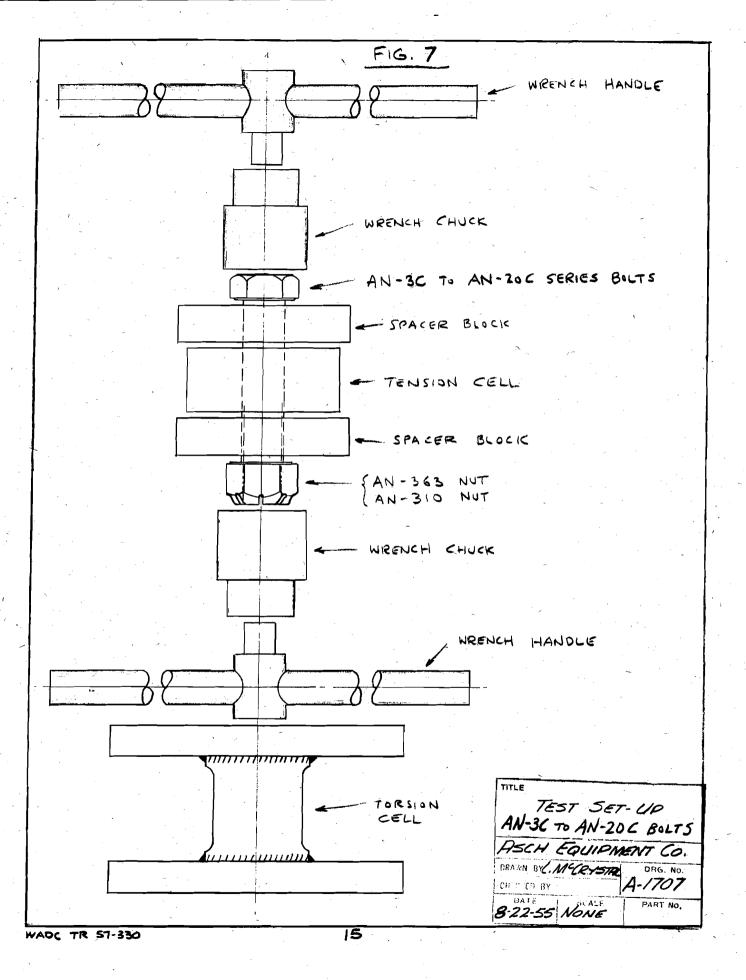


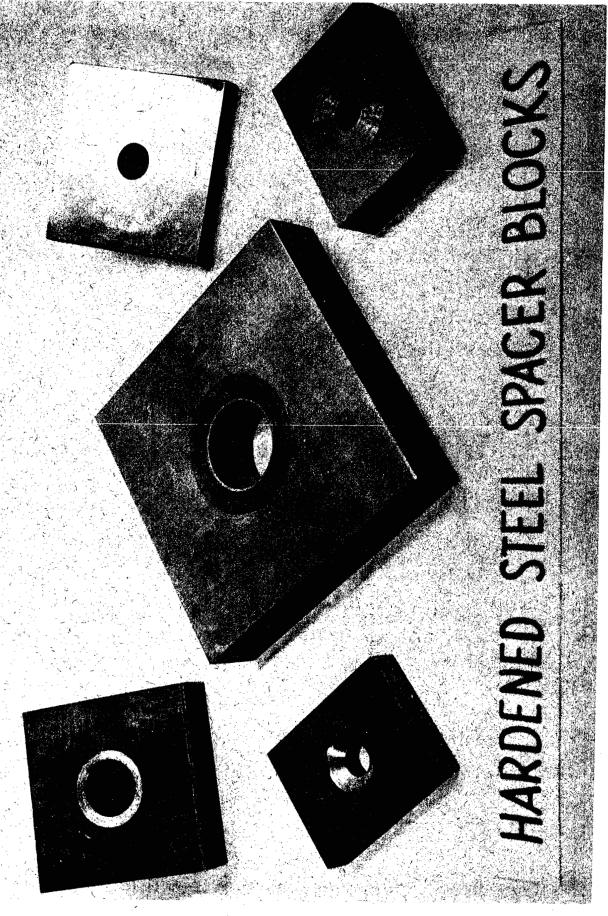




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## SECTION IV

## PRELIMINARY TESTING

TESTS OF TORQUING METHODS Initial experimental tests were made using AN-4C-30, 1/4-28 UNF-3A stainless steel bolts and AN-363-C428 silver plated steel nuts.

In these tests the compression recording strain gage cell was sandwiched between cold rolled steel spacer blocks drilled to accommodate the 1/4" diameter AN bolts. Bolts were torqued in the dry condition from the nut.

Two methods of obtaining torque-tension data for multiple torquings of the in ividual bolt-nut combinations were investigated.

- 1. Torquin the bolts to a maximum tension value (less than that causing bolt yield) in six uniform steps, returning to zero tension and repeating the sequence five times.
- 2. Torquing the bolts from zero tension to the first of six uniform steps five times in succession and repeating for each higher tension point up to the maximum tension.

Torquing to each tension value five times before proceeding to the next, required greater values of torque at the higher tension loads than did the method of torquing the bolt from minimum to maximum tension five times in succession. The spread between individual torque values for the same bolt tension, however, was not as great using method #2.

It was decided that method #1 would be adopted for the test program for the reason that torquing by this method was more representative of actual field conditions than method #2.

It was observed that the torque required for the same tension in the bolt over repeated runs increased greatly due to galling WADC TR 57-330 17

and scarring of the steel spacer blocks. Also, the initial run of each new bolt-nut combination increased over that of the previous combination as the surface of the spacer block became progressively rougher.

TESTING THE EFFECT OF WASHERS

In an effort to obtain more consistent results from bolt to bolt, hardened steel washers were inserted between the bearing surfaces of nut and bolt head and the steel spacer blocks. These washers, however, turned on the spacer block with the nut and caused the same galling conditions as did the nut turning directly on the spacer block.

Pinning the hardened washers to the spacer block proved unsatisfactory due to breakage of the brittle washers during the test runs.

TESTS TO EVALUATE HEAD & NUT BEARING FRICTION

In order to isolate the torque required to overcome thread friction from the torque required to overcome the friction of the nut and spacer block bearing surfaces, an AN-200-KP-4 ball bearing was mounted in the steel spacer block. The nut turned freely on the inner race of the ball bearing during these torque-tension tests. For this arrangement smaller torque values than previously observed were required to obtain the desired tension values in the bolts. After sixteen repeated dry torquing runs on the same bolt-nut combination the torque required to obtain the same tension in the bolt did not increase perceptibly. Thus for this bolt and nut combination the increase in thread friction due to repeated tightenings was negligible, indicating that the additional torque required for repeated tightenings, and successive bolts during previous tests was due principally to the worsening condition of the bearing surface of the steel spacer blocks, and nuts or heads.

TESTS
WITH
HARDENED
SPACER
BLOCKS

Since the surface condition of the cold rolled steel spacer blocks seemed to be the determining factor in the torque-tension relationship, and their reuse resulted in such wide fluctuations, it was decided to use SAE-Ol tool steel blocks hardened to Rockwell C-60 for the test program. It was expected that in this way each new bolt would be subject to the same conditions as the previous one without necessitating the use of a new set of spacer blocks for each individual bolt-nut test specimen. Although the hardened blocks were a distinct improvement over the cold rolled steel blocks, it was found that even the hardened blocks were subject to galling and smearing of metal, and required sanding.

Experimental tests using hardened steel (Rockwell C-60) spacer blocks and the following bolts and nuts were made.

- BOLTS: (1) AN8C-37, 1/2-20 UNF-3A Stainless Steel Bolt.
  - (2) 1/2" Diameter Standard Cold Finished Steel Bolt.
- NUTS: (1) AN-363-C820, 1/2" Silver Plated Steel Nut.
  - (2) 1/2" Standard Cold Finished Steel Nut.

These tests involved successive dry torquings from the nut for the various combinations of the above bolts and nuts, and torquings with the nut bearing surfaces alone lubricated with oil; with the threads alone lubricated with oil, and with both the thread and nut bearing surfaces lubricated with oil.

As a result of these tests the following conclusions were reached:

- 1. The increase in the torque requirements for successive tightenings of the same bolt-nut combination is due to the following factors:
  - (a) Increased friction between bearing surfaces of nut and hardened steel spacer block due to galling.

- (b) Increased friction between threads of the nut and bolt due to galling.
- 2. Factor (a) above accounts for a much greater percentage of the increased torque required after successive tightenings for the combinations tested.
- 3. A silver plated nut causes less galling of the hardened steel spacer block than does a standard steel nut. Silver plating acts like a lubricant in this respect.
- 4. The increase in torque values over successive dry tightenings of the stainless steel bolt and silver plated nut due to thread friction is negligible for as many as six torquings.
- 5. For the standard steel bolt used with the silver plated nut, or for the stainless steel bolt used with the standard steel nut the increase in torque values over successive dry tightenings is partially attributable to increased thread friction. That portion of the increased torque due to the increase in thread friction, however, is only about 10 to 20% of the total, the rest being due principally to the increased friction of the nut and spacer block bearing surfaces due to galling.

## SECTION V

## TEST PROCEDURES

TORQUE-TENSION TESTS Torque-tension tests were performed in the following order:

- 1. Torqued from nut Lubricated
- 2. Torqued from head Lubricated
- 3. Torqued from nut Dry
- 4. Torqued from head Dry

Each bolt specimen was torqued through its full range for five successive torquings before the next specimen was tested. All tests were made at room temperature. Readings were made as torque was increased. No determination was made of the torque due to the self locking provisions in the nuts at zero tension load. No release torque readings were made.

Torque values were recorded on the test data sheets for six increasing stress levels, wherever possible. On the fifth torquing the stress was raised to the computed yield point where possible, and the torque noted. In many cases principally during dry torquing from the head, the bolt failed before the higher tensile stress levels could be reached.

## LUBRICATED TORQUING

For the lubricated condition tests, thread compound, anti-seize, graphite petrolatum, Mil-T-5544 lubricant, which is a mixture of 50% graphite and 50% petrolatum, was applied to the threads and to the seating surfaces of the bolt heads and nuts prior to the initial torquing.

Lubrication was also applied during subsequent torquings due to loss of lubricant. The initial lubrication and subsequent lubrications

are noted in the "Test Data" sheets by an "L" placed before the torquing runs where they were applied.

For the MS-20,004 to MS-20,008 series bolts and the AN-3C to AN-8C series bolts, the seating surface of the spacer blocks had a ground finish at the start of the tests for each size bolt. No polishing or sanding was done on these surfaces during the lubricated torquing tests.

For the AN-509-8R to AN-509-816R series bolts, the finish was that left by the countersink tool at the start of the tests for each size bolt, and the surface was not processed in any way during the lubricated torquing tests.

For lubricated tests on the MS-20,009 to MS-20,024 bolts and for the AN-9C to AN-2OC bolts, and for the AN-509-916R screws, the seating surfaces of the spacer blocks were sanded after the fifth torquing of each bolt as described under dry torquing.

## DRY TORQUING

After completing the lubricated tests on a bolt size, the blocks and the specimens were thoroughly cleaned with carbon tetrachloride before dry torquing was begun.

It was found that the pressure of the seating surfaces of the bolts and nuts during dry torquing, deposited an increasing amount of metal and plating on the seating surfaces of the spacer blocks.

For this reason the bearing surface of the blocks were sanded after the fifth torquing on each bolt. Thus tests on each new specimen was started on a newly sanded surface. For the MS-20,004 to MS-20,024 series and the AN-3C to AN-20C series bolt spacers, and for the spacers used with the nuts of the AN-509-8R to AN-509-916R series

screws this was done on a belt sander using a "100-X Grit Metallic Cloth" manufactured by Behr Hanning of Troy, New York. For the AN-509-8R to AN-509-916R series bolt spacers used with the screw heads, this was done by hand sanding the countersunk area.

The "Test Data" sheets on finish show the Profilometer readings of these surfaces.

HARDNESS TESTS Hardness tests on the bolts were made by grinding a flat on the shank of the bolt. Tests on the nuts were made on the flats for hexagon nuts and on the seating surface for the EB and 42FW type nuts.

Spacer blocks hardness tests were made on the seating surfaces.

SURFACE FINISH TESTS Tests for surface finish were made on the spacer blocks in a direction across the cutting tool marks. In the case of the bolt and nut seating surface this was in a radial direction. For a few small sizes it was necessary to depart from the radial somewhat to clear the shank of the bolt.

## SECTION VI

## TEST RESULTS

Appendix II contains the data on the hardness and surface finish of the bolt heads, the nuts, and the spacer blocks.

Appendix III contains the "Test Data" sheets showing the torque-tension test results obtained with the various bolts and nuts for the different test conditions.

Appendix IV contains graphs of the relationship between the average torque and the tension for the various types and sizes of bolts, for the different conditions of test. Plot lines connect average points directly, without curve fitting. On Pages 166 to 175 are shown related families of curves for the various types of bolts tested.

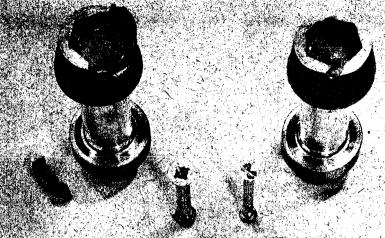


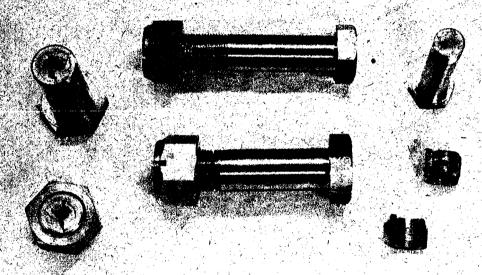
FIG. 9

EXAMPLES

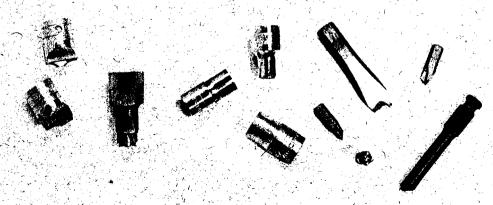
TEST SPECIMEN

TOOL FAILURES

BOLT HEAD RECESS RUPTURE



BOLT FAILURE IN SHEAR AT ROOT DIAMETER



DRIVING TOOL FAILURES

## SECTION VII

#### CONCLUSIONS

LUBRI CATED TORQUING Lubricated condition torquing produces average torque-tension relationships which do not vary appreciably over repeated torquings to the high tensile stress levels.

The torque tension relationship varies with different lubricants. Specification Mil-T-5544 lubricant possesses outstanding anti-friction and anti-seize properties, and lower torque values were required to produce a given tension than other lubricants tried.

DRY TORQUING The torque required to produce a certain tension in the bolts increased with each successive dry torquing, due principally to the progressive deterioration of the bearing surfaces under the head or nut.

A study of the data sheets indicates that the socket heads on the MS-20,004 to MS-20,024 series bolts, and the Phillips, Frearson and screwdriver slots on the AN-509-8R to AN-509-916R series screws, do not develop the full tension capabilities of these bolts and screws under conditions of dry torquing. In most cases the higher tensile stresses were not reached due to rupture of the heads by torquing.

In the case of the AN-3C to AN-2OC series bolts, this tendency to rupture the head was not evident, except in some isolated cases.

For the case of the AN-3C to AN-12C series bolts, the torque from the head was 50 to 100% greater than the torque from the silver plated nut, indicating the effectiveness of the plating.

TORQUE VARIATIONS AMONG INDIVIDUAL BOLTS The torque tension relationship among individual bolts of the same size in a series, showed an average variation from the mean of about ± 18% for both the dry and lubricated cases; with the exception of the dry torquing case for the MS-20,004 to MS-20,024 series bolts where the average variation was about 26%. These percentages were based on a 7% sample of all the results.

EFFECT OF CLEARANCE HOLES ON SPACER BLOCKS It was observed that torque values obtained during the dry torquing tests were dependent to a noticeable extent on the size of the clearance holes drilled in the spacer blocks to accommodate a particular diameter bolt. As the diameter of the hole is enlarged, the torque required increases also; due to the reduced bearing surface area, which increases the friction, galling and seizing between bolt head or nut and the spacer block. See galling areas on blocks in Fig. 8.

The torque data obtained during this test program thus pertains to the bolting of hardened steel plates through holes, which have the specific clearances noted on the "Data Sheets". See Appendix III. The relationships for other sizes of clearance holes were not investigated.

BEARING CONTACT AREA OF HEADS & NUTS Due to the fact that in most cases the bearing surfaces of both bolt heads and nuts are not formed flat and perpendicular to the bolt axis, the actual contact area is considerably different from that calculated from the dimensions shown on the specification sheets.

The heads of the AN-509-8R to AN-509-916R series flat head screws also do not fully contact the countersunk area of the spacer blocks. In most cases it is estimated that approximately 60% of the calculated bearing surface area was utilized.

EFFECT OF PLATING

Silver or cadmium plating on a bolt or nut acts as an anti-seize with regard to lowering the required torque values for the dry con-

ditions. Silver plating appears to be superior to cadmium plating with regard to its anti-seize effect. Under lubricated torquing conditions the effect of the plating on the torque required is greatly reduced.

Values of torque for dry nut torquing of the AN type bolts employing silver plated nuts may vary from lot to lot and from manufacturer, as a function of pre-plating surface finish, thickness of plating deposited, and plating techniques.

EFFECT OF DYED ALUMINUTS

After plotting the data obtained from the AN-509-8R to AN-509-1416R series screws with the NEJ aluminum nuts it was observed that for the case of dry torquing the curves did not follow the spread pattern obtained with the AN-365 silver plated steel nuts on the same size screws. Also the torque values were less. Compare graphs of bolts O, P and Q with W, X and Y.

These torque values were increased many fold when the blue dyed NMJ aluminum nuts were allowed to soak in carbon tetrachloride for about five minutes prior to testing. See graph of size X test bolt, Page 151.

The manufacturer of the blue dyed aluminum nuts later advised that these aluminum nuts were dyed blue for identification purposes only. During the process, the nuts are impregnated with a lubricant and are not subject to any subsequent bath or rinse that might tend to remove the lubricant.

The normal test procedure of wiping the nuts with carbon tetrachloride was not sufficient in this case to completely remove the lubricant and the results of the dry torquing test for bolts W, X and Y must be considered as having been modified by the manufacturers lubricant. STAINLESS STEEL BOLTS & NUTS Tests on the AN-14C to AN-20C type bolts, of 7/8" diameter to 1 1/4" diameter were run with AN-310 type unplated stainless steel nuts. The friction on the stainless steel threads between bolt and nut caused seizure and consequent failure of the bolt in shear at the root area during dry torquings at values of tension from 40-60,000 psi. See examples of specimen failures shown in Fig. 9.

The higher torque values attributable to thread friction appears to be due to the galling and seizing action caused by the use of stainless steel for both the bolt and the nut. This severe galling effect at the threads was not evident when both metals were dissimilar or one or both were plated.

SOCKET HEAD RUPTURE The recessed socket heads of the MS-20,004 to MS-20,024 type bolts ruptured before reaching the higher stress levels, when torquing from the head in the dry condition. Sizes between 1/2" diameter and 1 1/4" diameter ruptured out when torquing from the head in the dry condition at values of tension around 50,000 psi. With the 1 1/4" diameter and 1 1/2" diameter bolts under the same conditions, it was possible to torque to 70,000 psi. before rupture occurred.

Rupturing of the recessed head also occurred with the AN-509 flat head screws above 1/4" diameter, at values of 30,000 psi. or less. See Fig. 9.

DRIVE TOOL FAILURES In many cases, particularly with the AN-509 screws the best drive tools commercially available ruptured before the bolts could be torqued to the yield point. Some of these broken tools are shown in Fig. 9.

CONCLU-SION The torque-tension relationships as determined during these tests, must be regarded as applying only for the particular conditions of these tests. It was found that the bearing surfaces of the objects bolted together exercised considerable influence on the results obtained. Thus for spacers of other materials, with other hardness and finish treatment, and with different clearance in the bolt holes, other torque-tension relationships would be expected. The variance affects of these conditions are greatly magnified for the case of dry torquing.

In view of the much greater repeatability of lubricated torquing relationships, it would appear that this method would be preferred for pre-stressing, subject to a possible reduction in locking and holding resistance of the nut due to the thread lubrication.

During the preliminary tests, it was noted that most of the scatter and increase during torquing conditions was due to the nut or the head bearing surface friction and seizure. In view of this, a torquing procedure might be considered in which the lubricant is applied only under the nut or head, whichever is used for torquing, without lubricating the threads. This method would improve consistency of results over the totally dry case, and at the same time maintain the full locking resistance of the thread.

#### APPENDIX I

DIMENSIONAL DETAILS OF BOLTS TESTED

THREAD T

U x 45°

(a) CONCENTRICITY

.008 .0045

.006

-006

.006

.009

.012

Ù

.031 .005 .007 .0045

.Oh7

7با0ء .008 .010 .0045

.OL7 .009

.047 .010 .012 .006

.062

.062 .015 -018

.078

-091 .025 .032 .nna

.094

.094 .030 .039

.030 .089

.030 .089

.015 .077

.015 .077

.022 .030 .089

.022

.055

.055

1.625

1.750

1.875

X Y Z

.006

.011

.012 .016 .006

.018 .022

.020 .025

.022 .026 .009

.028 •035 .012

MT L-S-77L2

SPECIFICATION

1.005

1,001

1.131

1.126

1.256

.125 .055 .022

500

.547 .125

.594 .156

REFERENCE DIMENSIONS ARE FOR DESIGN PURPOSES ONLY AND ARE NOT AN INSPECTION REQUIREMENT. MATERIAL: ALLOY STEEL. SEE PROCUREMENT SPECIFICATION.

2.125 2.115

1.598 1,250 .667 .475

1.768 1.375

1.931 1.500

.746 .531

.823 .586

1.249

և.37և

.246 2.313

1.370 2.303

1.499 2.500 1.495 2.490

FINISH: CAIMIUM PLATE. SEE PROCUREMENT SPECIFICATION.

HEAT TREAT: SEE PROCUREMENT SPECIFICATION.

1-1/4 -12UNK-3A

1-3/8 -12UNF-3A

1-1/2 -12UNF-3A

ADD H BEFORE DASH NO. FOR BOLT WITH DRILLED HEAD,

EXAMPLES OF PART NOS.: MS20004-8

1/4-28 BOLT, 1.000 INCH LONG, .500 INCH GRIP, UNDRILLED HEAD. 1/4-28 BOLT, 1.000 INCH LONG, .500 INCH GRIP, DRILLED HEAD. 1/4-28 BOLT, 1.062 INCH LONG, .562 INCH GRIP, UNDRILLED HEAD. 1/4-28 BOLT, 1.062 INCH LONG, .562 INCH GRIP, DRILLED HEAD. MS2000LH8 M52000 Ju-9

BOLTS SHALL BE FREE FROM ALL HANGING BURRS AND SLIVERS WHICH MIGHT BECOME DISLODGED UNDER USAGE. COUNTERSINKING OF DRILLED HOLES IS OPTIONAL.

DIMENSIONS IN INCHES. UNLESS OTHERWISE SPECIFIED, TOLERANCES: DECIMALS ±.010, ANGLES ±1°.

MS20004 THRU CUSTODIAN Navy - Buler MS20024 BOLT - INTERNAL WRENCHING, 160,000 PSI PROCUREMENT SPECIFICATION SHEET Œ 2 MIL-B-7838

OTHER INTEREST: AIR FORCE

SUPERSEDES DRAWING WASLISS

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28

APPROVED

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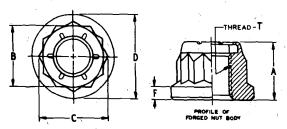
MS20022

MS2002L

related

ESNA

ELASTIC STOP NUT CORPORATION OF AMERICA, UNION, NEW JERSEY,



	THREAD -T
PROFILE O	F FULLY

ESNA PART NUMBER	THREAD	Α	В	C	D + 800	F	ULTIMATE TENSILE STRENGTH LB MIN (SEE PERFORMANCE)	APPROX WEIGHT LB/100	AVAILABILITY
EB-048	1/4-28NF-3	.344	.377 .362	. 409	.531	.090	7,132	1.00	
EB-054	5/16-24NF-3.	.406	.439 .424	.479	.593	.090	11,322	1.40	
EB-064	3/8-24NF-3	. 453	.503 .488	. 551	.687	.099	16,876	2.00	-
EB-070	7/16-20NF-3	.516	.565 .550	.622	.781	. 107	22,892	2.80	·
EB-080	1/2-20NF-3	.563	.628 .612	.692	.875	.118	30,555	3.50	
E8-098	9/16-18NF-3	. 625	.691 .675	.763	.968	. 127	34,800	4.50	
EB-108	5/8-18NF-3	.672	.785 .769	.870	1.062	.136	44,200	6.40	
EB-126	3/4-16NF-3	.781	.943 .927	1.049	1.250	. 185	64,700	11.00	·
EB-144	7/8-14NF-3	.953	1.067	1.188	1.438	.219	88,400	15.00	
EB-164	1-14NF-3	1.125	1.194	1.331	1.625	. 328	119,000	25.00	<u> </u>
EB-162	1 1/8-12NF-3	1.296	1.382	V.543	1.875	. 438	150,000	36.00	,
EB-202	1 1/4-12NF-3	±.031 1.406	1.507 1.490	1.685	2.125	.500	189,000	50.00	1
EB-222	1 3/8-12NF-3	1.531	1.633	1.830	1.000-020 2.313	.562	233,000	62.00	Δ
EB-242	1 1/2-12NF-3	1.656	1.821	2.048	2.500	.656	281,400	85.00	Δ

CODE: PART NUMBER DESIGNATES DOUBLE HEX HIGH TENSILE NUT AS SPECIFIED IN TABULATION ABOVE.

EXAMPLE: EB-064 = DOUBLE HEX, HIGH TENSILE NUT, TYPE EB, 3/8-24 THREAD.

MATERIAL: STEEL - AISI 4130 (AMS 6370) OR EQUIVALENT, THREAD SIZES 1/4 THROUGH 1/2.

STEEL - AISI 3140 OR EQUIVALENT, THREAD SIZES 9/16 THROUGH 1. STEEL - AISI 4340 (AMS 6415) OR EQUIVALENT, THREAD SIZES 1 1/8 AND LARGER.

FINISH: CADMIUM PLATE - FEDERAL SPEC QQ-P-416, TYPE 1, CLASS C.

(DLOCKING INSERT: RED NYLON - "ZYTEL" 101.

HARDNESS: ROCKWELL "C". 29-35. (SEE NOTE 1).

MAGNETIC PARTICLE INSPECTION: PARTS INDIVIDUALLY INSPECTED IN ACCORDANCE WITH MILITARY SPECIFICATION MILI-14668 AND DYED GREEN.

NAS353 NUT - DOUBLE HEX, HIGH TENSILE	В	PERFORMANCE	ESNA - STANDARD	
		NA\$353		LB PAGE 1 OF 2

ESNA

ELASTIC STOP NUT\_CORPORATION OF AMERICA, UNION, NEW JERSEY.

THREAD SQUARENESS: ESNA SPEC 405, GROUP 11, SIZES 1 4 THROUGH 1 2 ESNA SPEC 405, GROUP 1, SIZES 9.16 AND LARGER.

THREADS: MIL SPEC MIL-5-7742.

TOLERANCES: UNLESS OTHERWISE SPECIFIED: DECIMALS, ± .015

FRECHMANCE

TORQUE: - NASSSS EXCEPT THAT THE ELEVATED TEMPERATURE TEST MAXIMUM IS 150°F.

AXIAL TENSILE STRENGTH - THE AXIAL TENSILE STRENGTH LISTED IN THE TABLE ON PAGE 1 OF 2 IS EQUIVALENT TO 180,000 PSI AT THE MINIMUM PITCH DIAMETER OF THE BOLT THREADS, FOR SIZES

1/4 THROUGH 1/2.

FOR SIZES 9/16 AND LARGER THE FIGURES LISTED ARE EQUIVALENT TO A MINIMUM OF 160,000 PSI AT THE MINIMUM PITCH DIAMETER OF THE BOLT THREADS.

APPROVAL STATUS: TYPE EB IS ACCEPTABLE FOR USE ON AIRCRAFT IN ACCORDANCE WITH BUREAU OF AERONAUTICS
APPROVAL LETTERS 11472 AND 52353, DATED 15 FEB 49 AND 8 JUL 49, RESPECTIVELY, AND AIR
MATERIEL COMMAND APPROVAL LETTER MCREXA71 DATA 20 JAN 50.

APPLICATION: TYPE EB IS DESIGNED FOR HIGH TENSILE APPLICATIONS WHERE WEIGHT AND SPACE LIMITATIONS ARE MAJOR CONSIDERATIONS.

ESNA AVAILABILITY CODE:

\* - STANDARD PARTS NORMALLY CARRIED IN STOCK.

1 - STANDARD PARTS IN STOCK OR AVAILABLE WITHIN NORMAL DELIVERY SCHEDULES.

 A - STANDARD PARTS AVAILABLE WITHIN NORMAL DELIVERY SCHEDULES BUT FOR WHICH MINIMUM PRODUCTION RUN REQUIREMENTS ARE NECESSARY.

NT - PARTS WHICH CAN BE MADE AVAILABLE IN PROTOTYPE QUANTITIES BUT PROCUREMENT IN VOLUME SHOULD ALLOW FOR PRODUCTION TOOLING.

NOTES: 1. WHEN MEASURING ROCKWELL HARDNESS OF TYPE EB NUTS, IT IS NECESSARY TO CUT OFF THE ENTIRE LOCKING DEVICE, GRIND THE TOR OF THE NUT SMOOTH AND PARALLEL TO THE NUT SEATING SURFACE AND REMOVE THE CADMIUM PLATING FROM THE SEATING SURFACE. THE HARDNESS READING IS THEN TO BE TAKEN ON THE TOP OF THE NUT.

2. WITH THE EXCEPTION OF THE FOLLOWING SIZES, 9/16, 5/8, 3/4, 7/8, 1 AND 1 1/8, WHICH WILL ALWAYS BE MANUFACTURED AS FORGINGS, EB NUTS WILL BE MANUFACTURED AS EITHER FORGINGS OR FULLY MACHINED PARTS. RECARDLESS OF MANUFACTURING METHOD THESE PARTS ARE INTERCHANGEABLE BOTH WITH RESPECT TO ENVELOPE DIMENSIONS AND PERFORMANCE. THEY WILL BE SHIPPOINTERCHANGEABLY, DEPENDENT ONLY UPON CURRENT AVAILABILITY, UNLESS INSTRUCTIONS TO THE CONTRARY ARE RECEIVED FROM THE CUSTOMER.

33. REFER TO ESNA STANDARD DRAWING NATOL FOR A TWO-LUG HIGH TENSILE NUT DESIGN.

PERFORMANCE SPECIFICATION ESNA - STANDARD

NAS353
AS APPLICABLE NUT - DOUBLE HEX, HIGH TENSILE PAGE 2 OF 2

# 'DESIGNED for 550° F." FLEXLOC

AIRCRAFT TYPE
SIZES: Valte %" EXTERNAL
STYLE "A" WRENCHING LOCKNUT

WRENCHING LOCKNUT EXTERNAL



FLEXLOC

National Fine Thread Series "DESIGNED for 550° F."



in appearance from Style "A," illustrated on the preceding page. Differences are due solely to the manufacturing processes involved and in no way affect performance or ather characteristics of the lacknut. Both styles are approved for aircroft use under latest NAS specifications, and have tentative approval under the new MIL Specification. Style "B" FLEXLOC External Wrenching Locknuts shown on this page differ slightly

principle, Developed primority for dirframe assembly, they can be used to advantage in many other critical applications. High-strength A.M.S. 6280 minimum allay steel makes possible extreme tensiles with minimum weight. 12-point serrations for

standard bax or socket wrenches facilitate installation, even in close clearances.

FLEXIOCS, they are ane-piece, all-metal; incarparate the same efficient, self-locking

FIEXIOC External Wrenching Nuts are extra-performance locknuts. Like standard

External Wrenching Nuts are also stop nuts, lock securely anywhere an a bolt or stud without seating. Closely controlled torques provide positive locking without thread galling. Repeated re-use and high temperatures (550° F, and over) do not impair tocking efficiency. Approved under latest NAS Specifications, also tente-

STYLE B

ENCH	
1/2	
2	
NC1-3%	_
WRENCHING	VE THREAD (S.A.E.
EXTERNAL	NATIONAL FIN

STEEL, PLATED

EXTERNAL WRENCHING NUT-1/4 TO 1/4 INCH

NATIONAL FINE THREAD (S.A.E.)

A PART

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źź

tive approvals under new MIL Specifications

STYLE 'A

PACKING

TRINGLE

STEEL, PLATED

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4	Per In	1413	Further: Cad. Plane	•	2	J	-	HTAM	PLEXIOC Approx.	¥ ].	618	12.5
×	?		42FW-1216	1,250	787	.937	.185		00139	63400	30	· · š
*	2		42FW-1414	1.437	.953	1.06.1	219	088	87.600	84900	25	2
-	=	ю .	42FW-1614	1.625	1.125	1.187	266	9 'S 'V	117900	116900	23	78
	L							y -			Ĵ	1
2	72	m	42FW-1812	1.875	1.296	1.375	305	A MUI	148100	146800	25	=
7	12	•	42FW-2012	2.125	1.375	1.500	320	niniM	193700	185400	25	5
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ξ.	12		42FW-2412	2.500	1.625	1.812	375	915	286300	286300 275400	25	
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27100 34500 43800 8 These Parti are approved by both the Air Farce and Bureau of Acronoutics for aircraft use. • Present Notional Aircraft Standard

WHEN ORDERING-BE SURE TO SPECIFY QUANTITY . FLEXLOC PART NUMBER . THREAD SIZE 514 . 24 . 5

Sheet 619C-6

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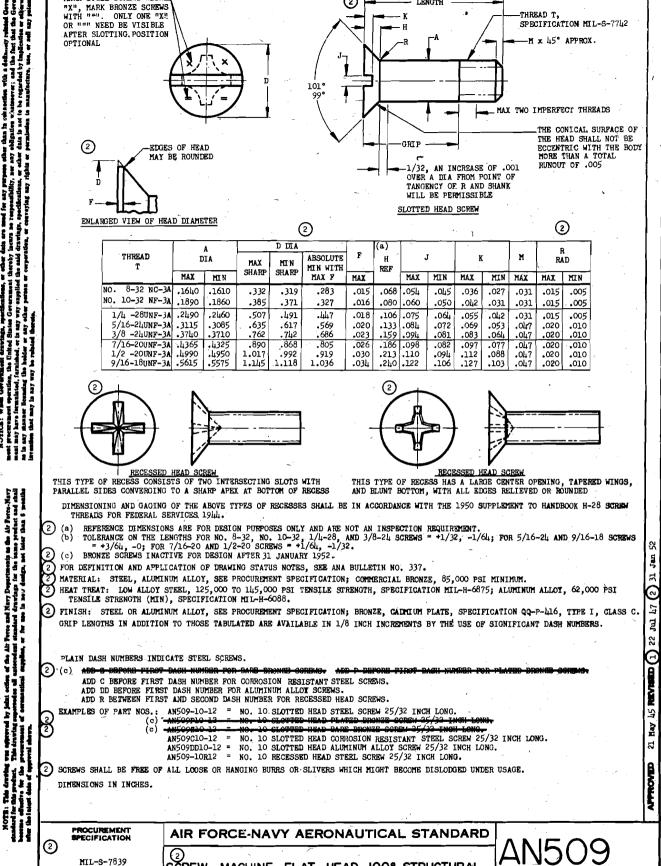
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WHEN ORDERING—BE SURE TO SPECIFY QUANTITY . FLEXLOC PART NUMBER . THREAD SIZE

34



MARK STEEL SCREWS WITH



②

LENGTH

SCREW-MACHINE, FLAT HEAD, 100°, STRUCTURAL

	FINE THR	EAD			1	
	D/	ash numbei	25		(a)	
	STEEL	OCOPPER BASE ALLOY	AL ALLOY	TAP T	A +.016	+.002 010
	448			NO. 4-48 NF-2	71,2	.250
(b)	640	B640	D640	No. 6-bu NF-2	.172	.312
	836	в636	p836	NO. 8-36 NF-2	.234	344
	1032	B1032	D1032	NO. 10-32 NF-3	.234	.375
	428	вц28	D428	1/4 -28 NF-3	.312	.438
	524	B524	D524	5/16-24 NF-3	.344	.500
	62և	B624	D624	3/8 -24 NF-3	.453	.563
	720	B720	D720	7/16-20 NF-3	.453	.625
	820	B820	D820	1/2 -20 NF-3	.594	.750
	918~	B918	D918	9/16-18 NF-3	.688	.875
	1018	B1018	D1018	5/8 -18 NF-3	.750	.938
	1216	B1216	D1216	3/4 -16 NF-3	.875	1.063
	1414	В1414	ըչկչկ	7/8 -14 NF-3	1.000	1.250
	1614	в1614	D1614	1 -14 NF-3	1.125	1.438
	1812	B1812	D1812	1-1/8 -12 NF-3	1.250	1.625
	2012	B2012	D2012	1-1/4 -12 NF-3	1.438	1.813

	COARSE TI	HREAD		•		
	0بئيا	Вило	Dirito	NO. 4-40 NC-2	.11.1	.250
	632	B632	D632	NO. 6-32 NC-2	.172	.312
	832	B832	D832	NO. 8-32 NC-2	.234	.344
	1057	B1024	D1024	NO. 10-24 NC-3	.234	.375
1	420	Bl <sub>1</sub> 20	D420	1/4 -20 NC-3	.312	.438
	518	D518	D518	5/16-18 NC-3	311	.500
	616	B616	D616	3/3 -16 NC-3	-453	.563
	714			7/16-14 NC-3	.453	.625
ı	813	B813		1/2 -13 NC-3	-594	.750
(b)	912	B912	1912	9/16-12 NC-3	.688	.875
- 1	1011	B1011	D1011	5/8 -11 NC-3	.750	.938
	1210 -	B1210	D1510	3/4 -10 NC-3	.875	1.063
1 .	1409	B1409	D17t05	7/8 - 9 NC-3	1.000	1.250
	1608	81608	p1608	1 -8 N-3	1,125	1,438
	1808	B1808	D1808	1-1/8 - 8 N-3	1.250	625
	2008	B2008	D2008	1-1/4 - 8  N-3	1.կ38	1.81

- (a) MINIMUM A NOT SPECIFIED. LIMITED ONLY BY STRENGTH REQUIREMENT OF SPECIFICATION.
- ◑ (b) Dash numbers 448 thru 836 and b640 thru b836 and d640 thru d836 for fine thread nuts and 1024 thru 2008 and b1024 thru B2008 AND D1021 THRU D2008 FOR COARSE THREAD NUTS INACTIVE FOR DESIGN AFTER 14 APRIL, 1949.
- FOR DEFINITION AND APPLICATION OF DRAWING STATUS NOTE SEE ANA BULLETIN NO. 337.
- ① ① ADD A AFTER TASH NUMBER FOR NUTS HAVING NON-METALLIC INSERTS.
- 1 ADD C AFTER DASH NUMBER FOR NUTS FABRICATED ENTIRELY FROM METAL.
- 1 EXAMPLES OF PART NUMBERS:

AN365-L28 = 1/4-28 STEEL NUT, EITHER ALL METAL OR WITH NON-METALLIC INSERT. AN365DL28 = 1/4-28 ALUMINUM ALLOY NUT, EITHER ALL METAL OR WITH NON-METALLIC INSERT. AN365-L28C = 1/4-28 STEEL ALL METAL NUT.

DIMENSIONS IN INCHES.

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oved by jobs orden of the Time That Day i sperredes all astonders standard diversing of convention explain, or for use in now it may be pet lets offset, between, at an early

FOR INSTALLATION INSTRUCTIONS SEE DRAWING ANDIOO68.

PROCUREMENT SPECIFICATION	AIR FORCE-NAVY AERONAUTICAL STANDARD	1 N 1 7 C E
an-n-5	1 NUT-SELF LOCKING, 250° F	AN365

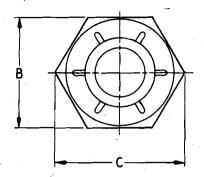
**GPO 821594** WADC TR 57-330 36

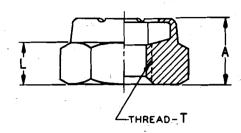
SUPERSEDES USAF DRAWING 365 AND NAF DRAWING 1137

REVISED (1) 14 Apr

3

ಭ APPROVED





ESNA PART NUMBER	THREAD	Α	<b>В</b>	C	REF
MJ-40	4-40NC-3B	.143	.252240	.275	081
MJ-62	6-32NC-3B	.178 ±.010	.314302	.344	.103
MJ-82	8-32NC-3B	.266	.346334	. 378	. 170
MJ-02	10-32NF-3	.266	.377365	.413	. 170
MJ-048	1/4-28NF-3	.345	.440428 -	. 488	.257

CODE: PART NUMBER AS LISTED IN THE TABULATION ABOVE DESIGNATES HIGH STRENGTH ALUMINUM ALLOY HEX NUT WITH FIBRE LOCKING INSERT.

PREFIX LETTER "N" TO PART NUMBER LISTED IN THE TABULATION ABOVE DESIGNATES HIGH STRENGTH ALUMINUM ALLOY HEX NUT WITH NYLON LOCKING INSERT.

EXAMPLE: MJ-02 = FIBRE LOCKING INSERT, HIGH STRENGTH ALUMINUM ALLOY HEX NUT, TYPE MJ, 10-32 THREAD. NMJ-02 = NYLON LOCKING INSERT, HIGH STRENGTH ALUMINUM ALLOY HEX NUT, TYPE MJ, 10-32 THREAD.

- MATERIAL: ALUMINUM ALLOY, 2014-T6 (AMS 4121).
   ALUMINUM ALLOY, 2024-T4 (AMS 4037) 1/4 SIZE ONLY.
   FINISH: ANODIZE, MIL SPEC MIL-A-8625(ASG) DYED BLUE AND LUBRICATED.
- LOCKING INSERT: RED FIBER

RED NYLON, "ZYTEL" 101.

THREAD SQUARENESS: ESNA SPEC 405, GROUP I.

THREADS: MIL SPEC MIL-S-7742.

TOLERANCES: UNLESS OTHERWISE SPECIFIED: DECIMALS, ± .015

PERFORMANCE: ESNA SPEC 414.

APPROVAL STATUS: PENDING QUALIFICATION UNDER APPLICABLE MS STANDARD DRAWINGS BEING COORDINATED

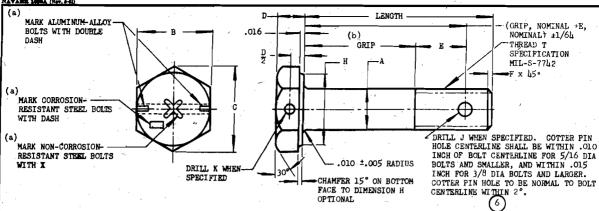
BY THE SERVICES AND INDUSTRY, APPROVAL FOR AIRCRAFT USE OF TYPE MJ NUTS AT STEEL LOADS MAY BE OBTAINED FROM EITHER THE BUREAU OF AERONAUTICS, FOR BUAER CONTRACTS, OR THE AIR MATERIEL COMMAND, FOR AIR FORCE CONTRACTS.

APPLICATION: TYPE MJ HIGH STRENGTH ALUMINUM ALLOY NUTS ARE DESIGNED TO BE USED IN PLACE OF STEEL

NUTS ON 125,000 PSI STEEL SCREWS IN ORDER TO EFFECT AN APPRECIABLE WEIGHT SAVING.

(SEE NOTE 1).

·		
PERFORMANCE SPECIFICATION	ESNA - STANDARD	N //
ESNA SPEC 414	NUT - HEX, MACHINE SCREW,	
25.07 57 20 1714	HIGH STRENGTH ALUMINUM ALLOY	PAGE   OF 2



												$\overline{}$		
BASIC AN PART	THREAD T	A DIA	A.	ı	3	C REF	Q		E REF	I	,	(c) H DIA	J DRILL DIA +.010	K DRILL DIA +.010
		MAX	MIN	MAX	MIN		MAX	MIN	У	MAX	MIN	MIN	000	-,000
AN3 AN4 AN5	NO. 10-32 NF-3A 1/4 -28 UNF-3A 5/16-24 UNF-3A	.189 .249 .312	.186 .246 .309	.377 .440 .502	.365 .428 .490	.430 .510 .580	.141 .172 .204	.109 .140 .172	5/16	.047 .047 .063	.015 .015	.359 .422 .484	.070 .076 .076	.046 .046 .070
AN6 AN7 AN8	3/8 -2h UNF-3A 7/16-20 UNF-3A 1/2 -20 UNF-3A	.374 .437 .499	.371 .433 .495	.565 .627 .752	.553 .615 .740	.650 .720 .870	.235 .266 .297	.203 .234 .265	31/64	.063 .063 .063	.031 .031 .031	.547 .609 .734	.106 .106 .106	.070 .070 .070
AN9 AN10 AN12	9/16-18 UNF-3A 5/8 -18 UNF-3A 3/4 -16 UNF-3A	.562 .62L .7L9	.558 .620 .7山	.877 .940 1.066	.865 .928 1.053	1.010 1.090 1.230	.328 .360 .422	.296 .328 .390	47/64	.078 .078 .078	.046 .046 .046	.859 .922 1.047	.141 .141 .141	.070 .07 <b>0</b> .070
ANIL ANI6	7/8 -14 UNF-3A 1 -14 NF-3A	.874 .999	.869 •993	1.253 1.441	1.240 1.428	1.կկ0 1.660	.485 .547	.453 .515		.094 .094	.062 .062	1.234	.141 .141	.070 .070
AN18 AN20	1-1/8 -12 UNF-3A 1-1/4 -12 UNF-3A		1.118 1.243	1.628 1.815	1.615	1.880 2.090	.610 .672		1-3/16 1-3/8	.110 .110	.078 .078	1.609	.141 .141	.070 .070

- SEE SHEET 3 FOR NOTES (a) AND (b).
- 6 THE DIAMETER OF THE WASHER FACE SHALL NOT EXCEED THE ACTUAL WIDTH ACROSS FLATS.

MATERIAL: NON-CORROSION-RESISTANT STEEL, CORROSION-RESISTANT STEEL OR ALUMINUM ALLOY. SEE PROCUREMENT SPECIFICATION.

SEE PROCUREMENT SPECIFICATION.

ADD C BEFORE DASH NUMBER FOR CORROSION-RESISTANT STEEL BOLT. ADD DD BEFORE DASH NUMBER FOR ALUMINUM-ALLOY BOLT.

ADD A AFTER DASH NUMBER FOR UNDRILLED BOLT. SEE ILLUSTRATION.

ADD H BEFORE DASH NUMBER FOR BOLT WITH DRILLED HEAD AND SHAME. SEE ILLUSTRATION.
ADD H BEFORE DASH NUMBER AND A AFTER DASH NUMBER FOR BOLT WITH DRILLED HEAD ONLY. SEE ILLUSTRATION.

#### EXAMPLES OF PART NUMBERS:

AN6-10 = 3/8 NON-CORROSION-RESISTANT STEEL BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED SHANK ONLY. SEE ILLUSTRATION.

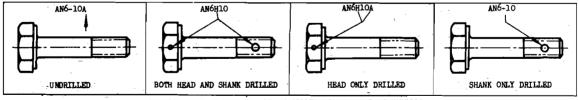
AN6DD10 = 3/8 ALUMINUM-ALLOY BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED SHANK ONLY. SEE ILLUSTRATION.

AN6DD10 = 3/8 ALUMINUM-ALLOY BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED SHANK ONLY. SEE ILLUSTRATION.

AN6DD10 = 3/8 ALUMINUM-ALLOY BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED SHANK AND HEAD. SEE ILLUSTRATION.

AN6DD10 = 3/8 ALUMINUM-ALLOY BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED HEAD AND SHANK. SEE ILLUSTRATION.

AN6DD10 = 3/8 ALUMINUM-ALLOY BOLT 1-5/64 LONG, 7/16 GRIP WITH DRILLED HEAD ONLY. SEE ILLUSTRATION.



#### ILLUSTRATION OF DRILLED AND UNDRILLED BOLTS AND PART NUMBERS

BOLTS SHALL BE FREE FROM ALL HANGING BURRS AND SLIVERS WHICH MIGHT BECOME DISLODGED UNDER USAGE. COUNTERSINKING OF DRILLED HOLES IN HEAD IS MANDATORY. COUNTERSINKING OF DRILLED HOLES IN SHANK IS OPTIONAL.

DIMENSIONS IN INCHES. UNLESS OTHERWISE SPECIFIED, TOLERANCES: DECIMALS ±.010, ANGLES ±5°.

PROCUREMENT SPECIFICATION AIR FORCE-NAVY AERONAUTICAL STANDARD AN3 THRU AN2O MIL-B-6812 BOLT - MACHINE, AIRCRAFT SHEET 1 OF h

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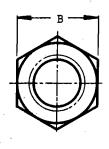
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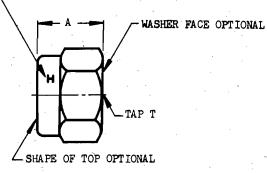
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APPROVED

MARK WITH H TO DESIGNATE HIGH-TEMPERATURE NUTS. POSITION OPTIONAL





#### FINE THREAD

	DASH NUI	MBERS		(a) (2)	(2),
COR RES	STEEL	COPPER BASE ALLOY	TAPT	+.016	+.002 010
C1032	1032	B1032	NO. 10-32 NF-3	.234	•375
C428	428	в428	1/4 -28 NF-3	.312	.438
C524	524	B524	5/16-24 NF-3	-344	.500
C624	624	B624	3/8 -24 NF-3	.453	.563
C720	720	B720	7/16-20 NF-3	.453	.625
C820	820	B820	1/2 -20 NF-3	.594	.750
C918	918	B918	9/16-18 NF-3	.688	.875
C1018	1018	B1018	5/8 -18 NF-3	.750	.938
C1216	1216	B1216	3/4 -16 NF-3	-875	1.063

(	2) COARSE TH	READ		• .		
•	C632	632	в632	No. 6-32 NC-2	.172	.312
_	C832	832	в832	No. 8-32 NC-2	.234	.344
Γ	6105/1	1024	B1024	No. 10-24 NC-2	1.234	315
	CH20	420	B420	1/4 -20 NC-3	732	.438
f	C518	518	B518	5/16-18 NC 5	.344	.500
	c616	616	B616	3/8 =16 NC-3	.453	.563
② (b)	C714	714	В714	7/16-14 NC-3	.453	.625
	C813	813	P813	1/2 13 NC-3	•594	.750
ĺ	.C913	ووو	В913	9/16-12 NC-9	.688	.875
	C1011	1011	B1011	5/8 -11 NC-3	750	.938
	c1210	1210	B1210	3/4 -10 NC-3	.875	1.063
•	-					

- (a) MINIMUM A NOT SPECIFIED. LIMITED ONLY BY STRENGTH REQUIREMENT OF SPECIFICATION.
- (b) DASH NOS. Clo24 THRU Cl210, 1024 THRU 1210, AND Bl024 THRU Bl210 FOR COARSE THREAD NUTS INACTIVE FOR DESIGN AFTER 14 APRIL 1949.
  - FOR DEFINITION AND APPLICATION OF DRAWING STATUS NOTE SEE ANA BULLETIN NO. 337.
  - EXAMPLES OF PART NUMBERS: AN363-428 = 1/4-28 STEEL NUT.

AN363B632 = NO. 6-32 COPPER BASE ALLOY NUT. AN363C $\pm$ 28 = 1/ $\pm$ -28 CORROSION RESISTING STEEL NUT.

DIMENSIONS IN INCHES.

FOR INSTALLATION INSTRUCTIONS SEE DRAWING ANDLOO68.

* *					
PROCUREMENT SPECIFICATION	AIR FORCE	- NAVY A	ERONAUTICAL	STANDARD	444565
AM-N-10	2	NUT - SELF	LOCKING, 550°F		AN363
	*				, 1 ×

SUPERSEDES USAF DRAWING 363

7

3

5

ROUND OR SQUARE BOTTOM CASTELLATION OPTIONAL

CHAMPER ON BOTTOM FACE 15° TO DIMENSION A OPTIONAL

THREAD T, SPECIFICATION AN-S-126.CSINK 110° TO OD OF THREADS

3

· · · · · · · ·	THREAD		ISILE STRENGTH	(a)	J B	() <sub>E</sub>	н	J	н	- R
AN PART NO.	T	STEEL	AL ALLOY	<b>- ^</b> ,	APPROX	•	, n	+1/32 -0	<b>,                                    </b>	
AN310- 3	NO. 10-32NF-3	2 210	1 100	.375 <sup>+.002</sup>	7/16	7/64	1/4	5/64	,110	3/32
AN310- 4	1/4 -28NF-3	4 080	2 030	.438+.002	1/2	1/8	9/32	5/64	.125	3/32
AN310- 5	5/16-24NF-3	6 500	3 220	.500+.002	37/64	11/64	21/64	5/64	.172	3/32
AN310- 6	3/8 -24NF-3	10 100	5 020	.563 <sup>+.002</sup>	21/32	7/32	13/32	1/8	.218	3/32
AN310- 7	7/16-20NF-3	13 600	6 750	.625+.002	23/32	17/64	29/64	1/8	.265	3/32
AN310- 8	1/2 -20NF-3	18 500	9 180	.750+.002	7/8	23/64	9/16	1/8	.359	1/8
AN310- 9	9/16-18 <b>nf</b> -3	23 600	11 700	.875+.002	1- 1/64	25/64	39/64	5/32	.390	5/32
AN310-10	5/8 -18NF-3	30 100	14 900	1.000+.002	1- 5/32	15/32	23/32	5/32	.468	5/32
AN310-12	3/4 -16NP-3	ht 000	21 800	1.125+.002	1-19/64	9/16	13/16	5/32	.562	3/16
AN310-14	7/8 <b>-14nf</b> -3	60 000	29 800	1.313+.002	1-33/64	21/32	29/32	5/32	.656	3/16
AN310-16	1 -14NF-3	80 700	40 000	1.500+.002	1-47/64	3/4	1	5/32	.750	3/16
AN310-18	1-1/8 -12NF-3	101 800	50 <b>500</b>	1.688+.002	1-61/64	13/16	1- 5/32	5/32	*81 <sup>1</sup> 1	1/4
AN310-20	· 1-1/4 -12NF-3	130 200	ert 1100	1.875+.002	2-11/64	7/8	1- 1/4	5/32	.938	1/4
		,								

(a) FOR AL ALLOY NUTS LARGER THAN -5 SIZE, TOLERANCES ON A MAY CONFORM TO APPLICABLE MATERIAL SPECIFICATIONS FOR BAR AND RCD. MATERIAL: STEEL, AL ALLOY AND CORROSION RESISTING STEEL. SEE PROCUREMENT SPECIFICATION.

FINISH: SEE PROCUREMENT SPECIFICATION.

ADD D BEFORE DASH NUMBER FOR AL ALLOY NUTS.

ADD C BEFORE DASH NUMBER FOR CORROSION RESISTING STEEL NUTS.

EXAMPLES OF PART NOS.: AN310-5 = STEEL NUT,  $5/16-2\ln F$ -3. AN310D5 = AL ALLOY NUT,  $5/16-2\ln F$ -3. AN310C5 = CORROSION RESISTING STEEL NUT,  $5/16-2\ln F$ -3.

③ REMOVE ALL BURRS.

DIMENSIONS IN INCHES. UNLESS OTHERWISE SPECIFIED, TOLERANCES: FRACTIONS ±1/64, DECIMALS ±.010, ANGLES ±1°

PROCUREMENT SPECIFICATION	AIR FORCE-NAVY AERONAUTICAL STANDARD	<b>ANI</b>
AN-N-2	O NUT-CASTELLATED, AIRFRAME	CVIA

40

25 May 44 (5) 51 Mar

(e)

REVISED (1) 4 Mar 44

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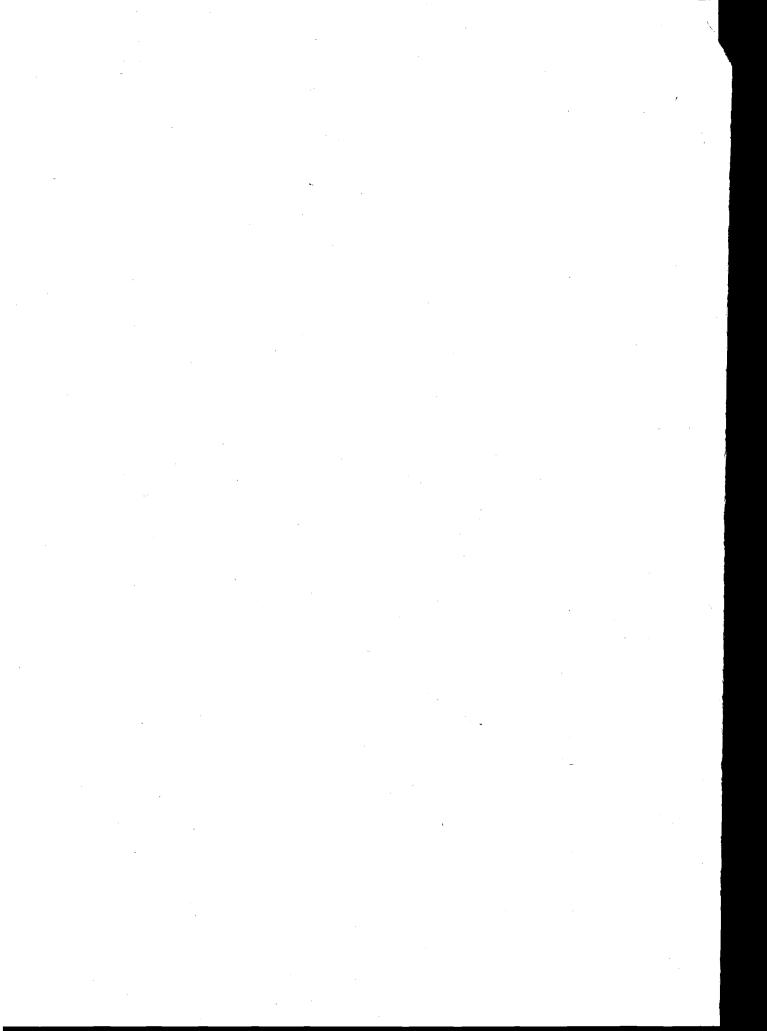
APPROVED

#### APPENDIX II

HARDNESS & SURFACE FINISH TEST DATA







DATA SHEET

OF NUTS SUPPLIED BY AIRCRAFT MANUFACTURERS WITH " ASCH EQUIPMENT CO. COMPARISON OF HARDNESS & SURFACE FINISH

: FINISH	42 FW	LOCKHEED AIRCRAFT CO.			- gap-philipson	24.3		32.1	39.0	32.3	25.3	72.2	
BEARING SURFACE FINISH RMS.	42 FW	BOEING LOCKHEED AIRPRAFE CO.	34.3	57.6	70.4	8	74.6	79.8	79.8	53.2	16 Francisco Control	52.5	9.09
ВЕЯК	EB NUTS	ASCH EQUIP. CO.	18.6	20.6	21.7	25.7	26.3	26.2	27.3	25.9	161	22.6	7:57
	42 FW	LOCKHEED AIRCRAFT CO.			*Andrones	56	a constitution of the cons	34	28	3/	62	38	appelline in the language
HARDNESS ROCKWELL'C'	42 FW	BOEING LOCKHEED PIREMANE CO. PURCRAFT CO.	35	36	33	56	33	33	30	3/	And The Control of th	3/	58
HA	EB NUTS	HSCH EQUIP. CO.	,0/	25	<i>E/</i>	"	27	20	90	77	31	32	39
	9.0	5/2 <b>6</b>	1/4	2/2	38	1/2	7/	110	8/5	8/2	%	*	1/1

#### — DATA SHEET SURFACE FINISH SPACER BLOCKS

GROUND	FINISH	SANDED	FINISH	MACHINE	D C'SINK FACE
SPACER	R.M.S.	SPACER	R.M.S.	SPACER	R.M.S.
37	10	9	24	16	85
<i>J</i> /	10	7	20	70	90
36	14	5	9	14	47
	//		15		50
35	5	/	19	12	NOT
	5	,	12	1/2	AVAILABLE
34	7	2B	14	10	50
	8	20	17		50
33	9	2Ac	13	12 A	NOT
	11 2	2176	13	12 A	AVAILABLE
32	13	18c	5	6	//
	9	700	フ		16.
3/	10	IAC	/8		12
	10	/// C	18	4	20
30	6	IAC	19	2	13
<i></i>	7		17		20
29	5	2Ac	14	10A	70 .
27	3	AHC	16	, , , ,	60
28	.4	2Bc -	16	8A	37
20	5	200	16	UA	28
TOTAL	162		302	2,4,6 £8A 10,10A,14£16	(157) (502)
AVERAGE	8.1	•	15.1	SPEC. 24,6 \$8A 19.6	SPEC.10,10A,14\$16 62.8
AVE.XI.33	10.8		20.1	26.1	83.5
				·	

NOTE: (1) READING CORRECTED TO PROFILOMETER CALIBRATION.

WADC TR 57-330

-- DATA SHEET --

HARDNESS & SURFACE FINISH

1. NUTS FURNISHED BY BOEING AIRPLANE CO. FOR COMPARSON 2. MFG. BY STD. PRESSED STEEL CO.

BOEING

	2	1							
A///7 A/9.	σu		HARONESS - KOCKWELL	たりこれ	157. 7731	SUK	SURFACE FINISH - RMS.	WISH-I	ems.
	/     	15. READING 2.48 READING	2.48 GROINS	70796	AVERAGE	157. READING	157 READING ZWO. READING	AVERAGE	"Ave. x1.33
	1	97	34	62		47	20		
10EW-018	7	28	34	1/2	$\times$	75	80	×	· ×
01/2 11/24	W	30	33	63		60	48	/	
			$\bigvee$	961	33			09	79.8
	`	26	26	25		00	65		
A7541,1010	7	3/	32	63	<u> </u>	45	55	$\times$	$\searrow$
0/0/-1/75	B	33	29	62		65	2		
		$\bigvee$		177	32			3	79.8
	\	28	32	60		27	35		
1101 IN 10V	7	30	28	58	$\times$	48	52	$\times$	$\times$
017/-N174	B	88	36	69		38	40	<u> </u>	
		$\bigvee$	$\bigvee$	181	3/			40	53.2
	\	28	33	19		32	35		
12 EW-161A	N	36	33	69	X	20	45	$\times$	$\times$
+101 1117+	W	26	32	28		35	90		/
		$\bigvee$	$\bigvee$	881	3/			39.5	52.5
	\	32	33	59		40	47		
10 Eul-1019	2	98	33	60	$\times$	37	48	$\times$	$\times$
7/0/ 1/74	3	35	38	73	7	47	55	<u>/</u>	/
		$\bigvee$	$\bigvee$	207	35			45.6	60.6
AMTO CO COCOCA	,	Concepto	10000	1				]	

-- CATA SHEET

HARDNESS & SURFACE FINISH

1. NUTS FURNISHED BY LOCKHEED AIRCRAFT CORP. FOR COMPARISON. 2.MFG. BY STO. PRESSED STEEL CO.

OKAFED

1117 110	SQ.		HARDNESS-ROCKWELL"C"	EDCKWE		SUK	SURFACE !	FINISH-RMS.	ems.
	٥		1 ST. READING 2 M. BADING	TOTAL	AVERAGE	187 BACANS	2 NO READING	AVERAGE "AVE. X 1.33	"ANE. X 1.33
	_	36	36	72		22	23		
10 EM - 018	N	35	34	69	X	25	20	×	$\rightarrow$
014	W	28	34	62		25	30	/	
				203	34			24.1	32.1
	1	52	28	53		23	30		
ATEM-1018	N	3/	32	63	$\times$	30	25	<u></u>	$\geq$
000/ 11/24	3	26	28	24		32	8		
		$\bigvee$		170	28		$\bigvee$	29.3	39.0
	/	29	3/	09		50	22		
10 EM -1911	N	30	29	59	X	30	24	$\times$	$\times$
0/7/ 14/ 74	n	32	37	69		25	25		
		$\bigvee$	$\bigvee$	188	3/			24.3	32.3
	/	3/	27	58		20	22		
12FW-1010	~	24	24	48	$\times$	23	6	$\times$	<u> </u>
t/t/ **/ **	W	30	$\alpha \varepsilon$	00		15	15		
		$\bigvee$		166	28	$\bigvee$		6/	25.3
-	1	27	3/	58		40	37		
125W-11.10	4	41	38	82	X	65	72	$\rightarrow$	$\rightarrow$
7/9/ 1/17	W	34	38	72		57	55		
		$\bigvee$	$\bigvee$	209	. 58	$\bigvee$		54.3	72.2
10010 10101	1								

NOTE: (1) READING CORRECTED TO PROFILOMETER CALIBRATION.

#### 

I. NUTS FURNISHED BY LOCKHEED AIRCRAFT CORP. & BOEING AIRPLANE CO. FOR COMPARISON, 2. MFG. BY STD. PRESSED STEEL CO.

NUT Nº	Sp	44	RDNESS 2 <sup>MO</sup> READING 24	ROCKH	IELL"C"	SUR	FACE FIL	VISH-R	M5.
7007 70	E <sub>C</sub> ,	IST. READING	2 NO READING	TOTAL	AVERAGE	151. READING	2 DREADING	HVERAGE	PAVE. X 1.33
	1	32	24	56		22	14		
42FW-720	2	28	32	60		22	17	$\times$	$\times$
LOCKHEED	3	31	29	60		15	20		
ZOCK/ACED				176	29			18.3	24.3
,	1	33	33	66		21	23		
42FW-428	2	37	38	75		22	32	$\times$	
BOEING	3	36	34	70		30	27		
BUEING				211	35			25.8	34.3
	1	34	31	65		55	43		
42FW-524	2	36	38	74		40	40	$\times$	$\times$
BOEING	3	38	37	75		37	45		
BUEING				214	36			43.3	57.6
, <u> </u>	1	34	32	66		5 <b>5</b>	52		
42 FW-624	2	33	29	62	$\rfloor$ , $\times$	70	65	$\times$	$\times$
BOEING	3	34	34	68		40	35		
BUEING .				196	33_			52.9	70.4
	1	35	28	63		35	42		1
									1 \
11 EW-720	2	31	32	63	$]$ $\times$	57	70	] X	
42 FW - 720	2 3	31 23	32 22	63 45		<i>57 52</i>	70 42	X	
42FW-720 BOEING		<del> </del>			29			49.6	66
		<del> </del>		45	29			49.6	66
BOEING		23	22	45 171	29	52	42	49.6	66
	3	23 33 32	35	45 171 68	29	52 35	42	49.6	66

NOTE: (1) READING CORRECTED TO PROFILOMETER CALIBRATION.

# -- DATA SHEET-

HARDNESS & SURFACE FINISH

\_\_\_\_\_SERIES BOLT

CODE Nº: A 20004-42

NUT Nº EB-048

SPACER Nº (2)- 1BC

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

MEDNESS.	~~~	. P V 14 C 15		<u> </u>	
ITEM.	SPEC. No	IST PEADING	2MOREADING	TOTAL	AVERAGE
		<i>3</i> 7	38	75	
BOIT	2	42	41	.83	$\rceil$
BOLT	3	41	38	79	
				237	40
	l	12	14	26	
N/1,	2	6	8	14	
NUT	3	9	10	19	
				59	10
SPACER	1.Bc	65	65	130	65
SPACER	1-BC	64	64	128	GA

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	IS READING	2º0 READING	AVERAGE	PAVE. X. 1.33
		8	14		
Boir	2	7	13		$\rightarrow$
BOLT	3	. 8	7		
	·			9.5	12.6
`		. //	14		
Kl. 17	2	13	15	$\times$	
NUT	3	/7	14		
				14	18.6
SPACER	1-Bc	()AVERAGE	RM.S. 20.1	SEE PAGE	
SPACER	1-BC	()AVERAGE	P.M.S. 20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# DATA SHEET

#### HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE No. B

AN STD. Nº MS 20005-50

NUT Nº <u>EB-054</u> SPACER Nº (Z)- ZAC

HAPDNESS: ROCKWELL "C"SCALE, 150 Kg. LOAD

IJEM.	SPEC. No	IST PEADING	2NOREADING	TOTAL	AVERAGE
		42	44	86	
80.7	2	22	22	44	
BOLT	3	39	39	78	1/ \
				208	35
	ĺ	20	26	46	
N / 1	2	26	26	52	
NUT	3	27	26	53	
				151	25
SPACER	2-Ac	65	65	130	65
SPACER	Z-AC	64	65	129	65

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	IS READING	200 READING	AVERAGE	AVE. x 1.33
		//	14		
Bay -	2	/3	13		
BOLT	3	//	11		
	/			12.1	16.1
		16	21		
N1,1-	2	15	16	$\sim$	
NUT	3	22	21		
				18.5	24.6
SPACER	2-Ac	() AVERAGE	RM.S. 20.1	SEE PAGE	
SPACER	2-Ac	(I)AVERAGE	P.M.S. 20.1	SEE PAGE	<u> </u>

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# -- DATA SHEET-

HARDNESS & SURFACE FINISH

MS	SERIES	BOIT
	ンドスにつ	

CODE No. C

AN STO. Nº:MS 20006-50

NUT Nº E8-064

SPACER Nº 2-BC & 2-B

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST. READING	2MDREADING	TOTAL	AVERAGE
	1	36	41	77	
BOIT	2	34	34	68	$7 \times $
BOLT	3	3/	3/	62	1/
				207	35
		12	15	27	
N. J	2	17	15	32	7 ×
NUT	3	10	11	21	
				80	13
SPACER	2-Bc	64	65	129	65
SPACER	2.8	65	65	130	<i>65</i>

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. x 1.33
		19	17		
Bar	2	18	16		
BOLT	3	13	13		
				16	21.3
		19	15		
N. 1	2	15	16	$\sim$	
NUT	3	14	19		
				16.3	21.7
SPACER	2.8c	() AVERAGE	RM.S. 20.1	SEE PAGE	
SPACER	2-B	(I)AVERAGE	P.M.S. 20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# ---DATA SHEET-

HARDNESS & SURFACE FINISH

MS\_\_\_SERIES BOLT

CODE NO D

NUT Nº E8-070

127

129

64

65

AN STD. Nº.MS 20007-50

SPACER Nº 2-Cc & 2.C

HAPDNESS ROCKWELL "C" SCALE, 150 Kg. LOAD							
ITEM.	SPEC. No	IST. PEADING	2MDREADING	TOTAL	AVERAGE		
	1 "	<i>38</i>	37	75			
BOLT	2	41	30	71			
COLI	3	40	41	81			
				227	38		
-		7	9	16			
NUT	2	10	14	24			
1401	3	11	13	24			

64

65

SURFACE FINISH (R.M.S.)

2-C

2-Cc

63

64

ITEM	SPECNO	S READING	2ºOREADING	AVERAGE	AVE. X 133
		14	12		
Boit	2	18	17	$\sim$	$\rightarrow$
BOLT	3	21	17		
				16.5	21.9
		17	15		
NUT	2	18	22	$\times$	
1401	3	24	20		
				19.3	25.7
SPACER			RM.S. 20.1		
SPACER	2-Cc	(I)AVERAGE	P.M.S. 20.1	SEE PAGE	

NOTE:

SPACER

SPACER

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# -DATA SHEET-

HARDNESS & SURFACE FINISH

\_\_\_\_\_SERIES BOLT

CODE Nº: E AN STD. Nº:MS 20008-50 NUT Nº <u>EB-080</u> SPACER Nº 2-DC & 2-D

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

THE DIALSO		77466		<u> </u>	
IJEM.	SPEC. No	IST PEADING	2NDREADING	TOTAL	AVERAGE
	1.	43	44	87	
BOLT	2	44	44	<i>88</i>	$\rceil \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$
	3	43	44	87	
				262	44
	1	21	24	45	
NUT	2	27	32	59	
1001	3	29	30	59	
				163	27
SPACER	2-0c	64	64	128	64
SPACER	2-0	63	63	126	63

SURFACE FINISH (R.M.S.)

ITEM	SPEC.No	S READING	2º0 READING	AVERAGE	PAVE. × 1.33
	. 1	15	18		
Bar	2	14	23	$\sim$	$\rightarrow$
BOLT	3	21	16		
				17.8	23.7
	1	18	23		
NUT	2	15	20	$\rightarrow$	
1701	3	18	25		
				19.8	26.3
SPACER	2-D c	() AVERAGE	RM.S. 20.1	SEE PAGE	
SPACER			P.M.S. 20.1		The second secon

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

## -DATA SHEET-

HARDNESS & SURFACE FINISH

\_\_\_\_\_ MS SERIES BOLT

CODE No. F

AN STD. Nº.MS 20009-50

NUT Nº E8-098

SPACER Nº 17 \$ 18

HAPDNESS: ROCKWELL "C" SCALE, 150 KG. LOAD

ITEM.	SPEC. No	IST PEADING	2NDREADING	TOTAL	AVERAGE
	1	36	35	71	
BOLT	2	42	41	83	$\rceil$
	3	37	- 39	76	
				230	3 <b>8</b>
	1	18	21	39	
NUT	2	3/	30	61	
7407	5	8	10	18	
				118	20
SPACER	17	54	57	111	56
SPACER	18	54	61	115	58

SURFACE FINISH (R.M.S.)

ITEM	SPEC.NO	15 READING	240 READING	AVERAGE	PAVE. x 1.33
	1	16	16		
BOLT	2	/3	20		
	3	19	22		
				17.5	23.3
	1	19	16		
NUT	2	26	26		
1701	3	15	16		
				19.7	26.2
SPACER	/7	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER			P.M.S20.1		

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# ---DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE Nº: G AN STD. Nº: M5 20010-50 NUT Nº EB-108 SPACER Nº 20 21

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

174200					
ITEM.	SPEC. No	IST PEADING	240 READING	TOTAL	AVERAGE
	I	38	39	77	
Boir	2	39	40	78	$\neg$
BOLT	3	39	40	19	1/ \
1				235	39
		34	28	62	
N / 1	2	30	30	60	$1 \times$
NUT	3	29	30	59	
				181	30
SPACER	20	57	<i>5</i> 5	112	56
SPACER	2/	<i>5</i> 7	60	//7	58.5

SURFACE FINISH (P.M.S.)

	7 2				
ITEM	SPECNO	S READING	2ºDREADING	AVERAGE	AVE. X 133
	1	26	15		
Boir	2	20	30		$\rightarrow$
BOLT	3	24	19		
	·			22.3	29.7
	1	21	23		
NUT	2	23	21	$\sim$	
1707	3	16	19		
				20.5	27.3
SPACER	20	OAVERAGE	RM.S20.1	SEE PAGE	
SPACER	21	()AVERAGE	P.M.S20.1	SEE PAGE	

NOTE:

(1) READING CORRECTED TO PROFILOMETER CALIBRATION.

## -DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE No. H

AN STD. Nº.MS 20012-50

NUT Nº E8-126

SPACER Nº 22824

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST PEADING	2 MOREADING	TOTAL	AVERAGE
	1.	45	45	90	
BOLT	2	41	42	83	
BOLT	3	44	45	89	]/ \
			262	44	
	t _	31	26	57	
N 81 5 mm	2	18	19	37	
NUT	3	16	17	33	]/ \
				127	21
SPACER	22	61	57	118	59
SPACER	24	59	55	114	57

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	PAVE. X 133
		12	/2		
BOIT	2	11	/3		
BOLT	3	15	14		
			/2.8	/7	
	1	22	25		
NUT	2	17	160	$\sim$	
1701	3	16	21		
				19.5	25.9
SPACER	22	()AVERAGE	RM.S20.1	SEE PAGE	
SPACER	24	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# -DATA SHEET-

HARDNESS & SURFACE FINISH

\_\_\_\_MS \_\_\_SERIES BOLT

Code No. I

NUT Nº E8-144

AN STO. Nº.MS 20014-50

SPACER Nº 25 6 27

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST READING	2NOREADING	TOTAL	AVERAGE
	1	40	41	81	
80.7	2	42	43	85	
BOLT	3	41	43	84	1/ \
				250	42
		37	38	75	
N / 1	2	24	30	54	$1 \times 1$
NUT	3	23	32	55	7/ \
				184	31
SPACER	25	60	59	119	60
SPACER	27	56	56	112	56

SURFACE FINISH (R.M.S.)

ITEM	SPECNO	15 REALING	200 READING	AVERAGE	PAVE. X 1.33
	- 1	18	13		
Bair	2	17	13		
BOLT	3	15	16		
				15.3	20.3
		14	13		
Klar	2	17	16	] ×	
NUT	3	16	13		
				14.8	19.7
SPACER	25	() AVERAGE	RM.S2011	SEE PAGE	
SPACER	27	(I)AVERAGE	R.M.S 20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# --- DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

Code No. J

AN STD. Nº MS 200/6-50

NUT Nº EB-164 SPACER Nº 28 6 29

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC Nº	IST PEADING	240 READING	TOTAL	AVERAGE
		42	42	84	
00-	2	41	41	82	7 ×
BOLT	3	43	42	85	
	251	42			
		29	33	61	
A /	- 2	33	33	66	
NUT	3	35	32	67	
				194	32
SPACER	28	67	67	134	67
SPACER	29	56	57	113	57

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2"DREADING	AVERAGE	AVE. × 1.33
		27	30		
Ban -	2	30	25		$\rightarrow$
BOLT	3	32	33		
			29.5	39.2	
		13	19		
N.L.	2	17	15	$\times$	
NUT	3	19	19		
				/7	22.6
SPACER.	28	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	29	MAVERAGE I	P.M.S20.1	SEE PAGE	

#### NOTE:

(1) READING CORRECTED TO PROFILOMETER CALIBRATION.

## -- DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE No. K

AN STO Nº MS 20018-50

NUT Nº E8-182

SPACER Nº 305 31

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

_					<del></del>
ITEM.	SPEC. No	IST READING	2MPREADING	TOTAL	AVERAGE
		42	44	86	
BOLT	2	42	43	85	$\neg$
BOLT	3	43	43	86	7/ \
				257	43
		39-	40	79	
A 1	2	<i>38</i>	39	77	7 ×
NUT	3	39	38	77	
				233	39
SPACER	30	60	64	124	62
SPACER	3/	54	58	112	56

SURFACE FINISH (R.M.S.)

ITEM	SPEC.No	15 READING	2º0 READING	(1) AVERAGE	AVE. x 1.33
		16	9		
<b>2</b> -, -	2	14	14		
BOLT	3	14.	17		
				16	21.3
	- 1 - 1 - 1 - 1	21	20		
N1. 1-	2	15	21	$\rightarrow$	
NUT	3	22	17		
				19.3	25.7
SPACER	30	() AVERAGE	RM.520.1	SEE PAGE	
SPACER	3/	(1)AVERAGE	R.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

## -- DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE Nº \_\_\_\_

AN STO. NºMS 20020-50

NUT Nº E8-202

SPACER Nº 32 8 33

HAPDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST PEADING	2NPREADING	TOTAL	AVERAGE
	1	44	44	88	
	2	44	40	84	
BOLT	3	40	43	83	1/ \
· ·				-	43
		30	<i>3</i> 3	63	
·	2	34	34	68	
NUT	3	27	29	56	
				187	31
SPACER	32	59	5 <b>5</b>	114	57
SPACER	33	59	59	118	59

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	2º0 READING	AVERAGE	AVE x 133
		9	//		
Rait	2	9	8	$\rightarrow$	
BOLT	3	6	6		
				8.2	10.9
·	1	48	50		
NICIT	2	42	45		$\rightarrow$
NUT	3	45	45		
				45.8	60.9
SPACER	32	(I) AVERAGE	RM.S20.1	SEE PAGE	
SPACER	33	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# --- DATA SHEET-

# HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE Nº M AN STD. Nº MS 20022-50 NUT Nº <u>EB-222</u> SPACER Nº 34 £ 35

HAPDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

NOCEWELL SCALE							
ITEM.	SPEC. Nº	IST PEADING	240READING	TOTAL	AVERAGE		
	l	36	<i>38</i>	74			
BOIT	2	42	42	84			
BOLT	3	38	38	76			
				74 84 76 234 56 57 58 171 123	39		
		27	29	560			
N/OF	2	<i>28</i>	29	57			
NUT	3	29	29	<i>58</i>			
				171	28.5		
SPACER	34	60	63	/23	62		
SPACER	35	62	66	128	64		

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. x 1.33
		17	15		
Bar	2	16	14	$\sim$	$\rightarrow$
BOLT	3	13	16		
				15.1	20.1
		52	60		
NUT	2	60	53	$\sim$	$\rightarrow$
1701	3	40	40		
				51	67.8
SPACER		()AVERAGE	RM.S20.1	SEE PAGE	
SPACER		(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# -DATA SHEET-

HARDNESS & SURFACE FINISH

MS SERIES BOLT

CODE No. N

NUT Nº EB-242

AN STD. Nº MS 20024-50

SPACER Nº 36 8 37

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

IJEM.	SPEC. No	IST. PEADING	2NOREADING	TOTAL	AVERAGE
		38	39	77	
BOIT	2	40	40	80	
BOLT	3	39	41	30	
<u> </u>	-			237	39.5
NuT		28	24	52	
	2	29	31	60	
	3	29	31	60	
				172	28.6
SPACER	36	63	66	129	65
SPACER	37	58	61	119	60

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2ºDREADING	AVERAGE	AVE × 1.33
		14	14		
Box	2	13	12		$\rightarrow$
BOLT	3	12	12		
	į			12.8	17
NUT		55	60		
	2	55	50		
	3	45	40		
				5/	67.8
SPACER		(I) AVERAGE	RM.S20.1	SEE PAGE	
SPACER		(I)AVERAGE	P.M.S20.1	SEE PAGE	` .

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

## -- DATA SHEET-

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

Code No. O

NUT Nº AN 365-832

AN STD. Nº AN 509-8R37

SPACER Nº 162

MARDNESS ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SUE Nº	15T. PEADING	2NDREADING	TOTAL	AVERAGE
	1	29	3/	60	AVERAGE
	2	35	32	67	7
BOLT	3	29	29	58	
				185	31
NúT		37	22	59	
	2	19	16	<i>35</i>	
	3	20	22	42	
				136	23
SPACER	1	59	59	118	59
SPACER	2	59	61	120	60

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. x 133
BOLT		22	25		
	2	<i>5</i> 7	60	$\rightarrow$	
	3	45	38		
				41.1	54.7
NUT		11	14		
	2	20	15	$\rightarrow$	
	3	22	18		
				16.6	22./
SPACER	1	() AVERAGE	PM.S20.1	SEE PAGE	
SPACER	2	()AVERAGE I	P.M.S26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# -DATA SHEET-

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE Nº. P AN STD. Nº. AN 509-10R37

NUT Nº AN 365-1032 SPACER Nº 3 & 4

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

	1,000,100,000						
IJEM.	SPEC. No	IST READING	240READING	TOTAL	AVERAGE		
	١	35	36	7/			
BOIT	2	33	34	67	$\rceil$		
BOLT	3	32	34	66			
				204	34		
NUT	1	21	22	43			
	2	22	21	43			
	3	23	22	45			
				131	22		
SPACER	3	63	63	126	63		
SPACER	4	62	63	/25	63		

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	240 READING	AVERAGE	PAVE. x. 1.33
BOLT	1	15	/7		
	2	/2	10	$\rightarrow$	$\rightarrow$
	3	15	17		
				14.3	19
NuT		26	<i>3</i> 3		
	2	18	25	$\times$	$\rightarrow$
	3	26	19		
				24.5	32.6
SPACER	3	()AVERAGE	RM.S20.1	SEE PAGE	
SPACER	4	(I)AVERAGE	P.M.S26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

## DATA SHEET-

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE No. Q AN STD. Nº AN 509-416 R 37 SPACER Nº 5 6 6

NUT Nº AN 365-428

HAPPNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

				- 142
SPEC. No	IST PEADING	2MDREADING	TOTAL	AVERAGE
١	<i>35</i>	36	71	
2	32	<i>3</i> <b>3</b>	65	$]$ $\times$
3	33	31	64	
			200	3 <b>3</b>
1	18	17	35	
2	11	9	20	
3	18	18	36	
			91	15
5	63	63	126	63
6	63	64	127	64
	3	2 32 3 33 1 18 2 11 3 18 5 63	1     35     36       2     32     33       3     33     31       1     18     17       2     11     9       3     18     18       5     63     63	1     35     36     7/       2     32     33     65       3     33     31     64       200     200       1     18     17     35       2     11     9     20       3     18     18     36       91       5     63     63     126

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	PAVE. X. 133
		22	17		
Bour	2	11	13		
BOLT	3	12	12		
				14.5	19.3
	1	12	13		
NICIT	2	18	24	$\sim$	
NUT	3	17	20		
				17.3	23
SPACER	5	() AVERAGE	RM. S20.1	SEE PAGE	
SPACER	6	(I)AVERAGE	P.M.S26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 500 SERIES BOLT

CODE Nº R AN STD. Nº RN 509-516 P48

NUT Nº 9N365-524 SPACER Nº 7 6 8

HAPPINESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

	14				7-12
ITEM.	SPEC. No	IST READING	240READING	TOTAL	AVERAGE
		3 <b>5</b>	36	70	
BOLT	2	35	35	70	
BOLT	3	ę			7/
				140	35
	ĺ	27	27	54	
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2	25	25	50	
NUT	3				
				104	26
SPACER	7	64	64	128	64
SPACER	8	65	66	/3/	66

SURFACE FINISH (P.M.S.)

00/4/7/00			_		
ITEM	SPECNO	15 READING	2 NO READING	AVERAGE	AVE. x 1.33
		23	15		
BOLT 2	21	17			
	3				
				19	25.3
		19	20		
Klast .					
1401	3				
				22	29.3
SPACER		()AVERAGE		SEE PAGE	
SPACER	8	(I)AVERAGE	P.M.S. 26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE No. 5 AN STD. No. AN 509-616 R 48 NUT Nº AN 365-624 SPACER Nº 9610

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

770/42	~~~				
ITEM.	SPEC. No	IST PEADING	24DREADING	TOTAL	AVERAGE
	1	29	29	58	
80.7	2	29	3/	60	$\neg$
BOLT	3	30	31.	61	
				179	30
		14	18	32	
N.J. :	2	20	24	44	$7 \times$
NUT	3	22	24	46	
				122	20
SPACER	9	61.	58	119	60
SPACER	10	66	66	132	66

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	240 READING	AVERAGE	PAVE. X 1.33
		18	21		
Boy	2	36	21	$\rightarrow$	
BOLT	3	25	20		
				23.5	31.3
, , , , , , , , , , , , , , , , , , ,		28	25		
NI.	2	25_	30		
NUT	3	27	26		
				26.8	35.6
SPACER	9	() AVERAGE	RM.5 20.1	SEE PAGE	
SPACER	10	(I)AVERAGE	P.M.S. <b>-83</b> .5	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

NUT Nº AN 365-720 SPACER Nº 1/6/2

HAPDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM	SPEC. Nº	IST READING	2NDREADING	TOTAL	AVERAGE
``	١	30	28	5 <b>8</b>	
BOIT	2	29	29	58	
BOLT	3	29	30	59	7/ \
				175	29
′		26	29	55	
A /	2	28	3/	59	$1 \times$
NUT	3	28	26	54	7/
				168	28
SPACER		63	62	125	62.5
SPACER	12	62	63	125	62.5

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	1ST READING	2º0 READING	AVERAGE	PAVE. X. 1.33
		22	32		
Boir	2	45	48	$\sim$	$\sim$
BOLT	3	60	43		
-				. 41.7	55.5
	. 1	23	28		
Klar	2	25	28		
NUT	3	22	17		
	·			23.8	31.7
SPACER	11	() AVERAGE	RM.S 20.1	SEE PAGE	
SPACER	/2	(I)AVERAGE	P.M.S26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE No. U

NUT Nº AN 365-820

AN STD. Nº AN 509-816 P49

SPACER Nº 136 14

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST READING	2NDREADING	TOTAL	AVERAGE
	1	32	36	68	
BOLT	2	36	37	73	
DOLI	3	36	38	74	
,				215	36
-	1	19	21	40	
N/1	2	19	21	40	
NUT	3	/7	20	37	
_				117	20
SPACER	13	64	64	128	64
SPACER	14	64	66	130	65

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2ºDREADING	AVERAGE	PAVE. X 1.33
		22	19		
Bout	2	22	21		
BOLT	3	27	22		
				22.1	29.4
		160	20		
NICE	2	20	20	$\rightarrow$	
NUT	3	22	24	20.3 SEE PAGE	
				20.3	27
SPACER	13	() AVERAGE	RM.S 20.1	SEE PAGE	
SPACER	14	(I)AVERAGE	P.M.S26.1	SEE PAGE	<u> 1900 - Marie Barrellon, Albertania de la compania del compania del compania de la compania del la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania del la compan</u>

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE No. V

NUT Nº AN 365-918

AN STD. Nº. AN 509-916 R52

SPACER Nº 15 8 16

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

17.70	محب ب				~ <del></del>
ITEM.	SPEC. No	IST READING	240READING	TOTAL	AVERAGE
	1	33	35	68	
BOLT	2	32	35	67	$\supset$
COLI	3	32	35	67	7/
				202	34
/	1	15	16	3/	
NUT	2	19	20	39	$\neg$
1001	3	17	16	33	
				103	17
SPACER	15	63	64	127	64
SPACER	16	46	51	97	49

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2" READING	VAVERAGE	AVE. x 1.33
		3 <b>8</b>	32		
BOLT	2	37	33	$\sim$	$\sim$
0001	3	27	30		
				32.8	43.6
		22	25		
NUT	2	28	37		$\rightarrow$
1701	3	27	23		
				27	35.9
SPACER	15	()AVERAGE	RM.S20.1	SEE PAGE	
SPACER	16	()AVERAGE	P.M.S83.5	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

AN STD. Nº AN SOO BR37

NUT Nº NMJ-82 SPACER Nº 162

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

MEDIALOU.	~~~				,,-\ <u></u>
ITEM.	SPEC. No	IST. READING	2MPREADING	TOTAL	AVERAGE
	1	21	29	50	
BOLT	2	32	34	66	
BOLT	3	31	33	64	7/ \
				180	30
	1	7	7	14	
A/	2	9	9	18	$\neg$
NUT	3	8	5	13	
•				45	8
SPACER	/	59	59	118	59
SPACER	2	- 59	61	120	60

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. X 133
		41	30		
Box	2	40	40	$\sim$	
BOLT	3	30	32		
				<b>35</b> ,5	47.2
		4	3		
NI	2	5	5	$\times$	
NUT	3	4	4		
				4.2	5.6
SPACER			RM.S. 20.1		
SPACER	2	()AVERAGE	R.M.S. 26.1	SEE PAGE	,

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

CODE Nº. X AN STD. Nº. AN 509 10 R37 NUT Nº NMJ-02 SPACER Nº 354

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

MAKUNESS:	ROCK	WELL_	DEALE, 19	<u> </u>	
ITEM.	SPEC. Nº	IST. READING	2 MDREADING	TOTAL	AVERAGE
	l l	<i>32</i>	34	66	
BOLT	2	29	34	63	
BOLT	3				7/ \
				129	32
*		9	9	18	
* A1	2	5	6	11	
NUT	3			,	
-				29	7
SPACER	3	63	63	126	63
SPACER	4	62	63	125	63

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. X 1.33
		14	. /7		
Boir	2	//	14	<b>X</b> .	$\rightarrow$
BOLT	3	·			
				14	18.6
		12	10		
N1/:-	2	8	8	$\rightarrow$	
NUT	3				
				9.5	12.6
SPACER		The second secon	RM.S20.1		
SPACER	4	(I)AVERAGE	RM.5:-26.1	SEE PAGE	·

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN 509 SERIES BOLT

AN STD. Nº. AN 509 416 R37

NUT Nº NMJ-048 SPACER Nº 556

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

11-11-11-11-11	140 040				7-12-
ITEM.	SPEC. No	IST BEADING	2MPREADING	TOTAL	AVERAGE
		34	35	69	
BOIT	2	34	34	68	
BOLT	3	33	33	66.	
<u> </u>				203	34
		10	9	19	
A /	2	11	10	21	
NUT	5	9	9	18	
				58	10
SPACER	5	63	63	126	63
SPACER	6	63	64	127	64

SURFACE FINISH (R.M.S.)

ITEM	SPEC.NO	15 READING	2 NO READING	AVERAGE	AVE. x 1.33
		12	10		
Boir	2	11	14		
BOLT	3	16	18		
·				13.5	18
		10	8		
NI.	2	7	9	$\rightarrow$	
NUT	3	10	9	13.5 8.8 SEE PAGE	
				8.8	11.7
SPACER		()AVERAGE		SEE PAGE	
SPACER	6	(I)AVERAGE	R.M.S26.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº. A-A

AN STD. Nº. RN 3C-30

NUT Nº AN 363 C1032 SPACER Nº (2-1AC

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST READING	2MDREADING	TOTAL	AVERAGE
	1	30	28	58	
BOLT	2	29	30	59	
COL	3	29	30	59	7/ \
				176	29
·		20	23	43	
N. l	2	19	24	43	$1 \times$
NUT	3	25	26	51	
· · · · · · · · · · · · · · · · · · ·				137	23
SPACER	1-Ac	65	65	130	65
SPACER	1-AC	65	65	130	65

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	IS READING	2ºDREADING	(1) AVERAGE	PAVE. X 133
		9	12		
Bar	2	9	13		
BOLT	3	10	14		
				//. Z //7. Z SEE PAGE	14.9
		16	21		
NICE	2	17	17	$\rightarrow$	
NUT	3	15	17		
•				17.2	22.9
SPACER	1-Ac	() AVERAGE	RM. S 20.1	SEE PAGE	
SPACER	1-Ac	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº. B-8

AN STD. Nº. AN QC-30

NUT Nº AW363 C-428 SPACER Nº (2) - 18 C

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

	14004				
ITEM.	SPEC. No	IST. READING	2 MOREADING	TOTAL	AVERAGE
	١	34	35	69	
1000	2	32	35	67	
BOLT	3	35	35	70	
				206	34
	1	30	28	58	
	2	27	26	53	$] \times  $
NUT	3	26	26	52	
				163	27
SPACER	1-Bc	65	65	130	65
SPACER	1-Bc	64	64	128	64

SURFACE FINISH (P.M.S.)

ITEM	SPEC.NO	S READING	200 READING	AVERAGE	OAVE. x 1.33
		/2	18		
B	2	13	11	$\sim$	$\times$
BOLT	3	10	7		
	1 17 16	15.7			
· · · · · · · · · · · · · · · · · · ·	1	17	16		
NI.	2	20	20	$\times$	$ $ $\times$ $ $
NUT	3	15	2/		
				18.1	24.1
SPACER		()AVERAGE		SEE PAGE	
SPACER	1-Bc	(I)AVERAGE	R.M.S20.1	SEE PAGE	

Nors:

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

\_\_\_AN SERIES BOLT

CODE Nº: C-C AN STD. Nº: AN 5C-35 NUT Nº AN 363C-524 SPACER Nº (2) - 2AC

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

1000					
ITEM.	SPEC. No	IST. PEADING	2 MOREADING	TOTAL	AVERAGE
	l	36	37	73	
BOIT	2	34	33	67	
BOLT	3	33	32	65	
· 				205	34
	1	<i>32</i>	32	64	
N/0 -	2	29	28	57	
NUT	3	31	3/	62	
				183	3/
SPACER	2-Ac	65	65	130	65
SPACER	2-Ac	64	65	/30	65

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	240 READING	AVERAGE	PAVE X 133
		8	5		
Boil	2	7	11	$\times$	$\times$
BOLT	3	5	6		
				7	9.3
		19	21		
NI	2	23	21	$\rightarrow$	$\rightarrow$
NUT	3	22	19		
<u> </u>				20.9	27.8
SPACER		A STATE OF THE PARTY OF THE PAR	PM.S 20.1	the same and the s	
SPACER	2-AC	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

### -DATA SHEET

HARDNESS & SURFACE FINISH

SERIES BOLT

CODE Nº: 0-0

AN STD. Nº: AN 6C-36

NUT Nº AN 363C-624 SPACER Nº 28C & 28

HAPDNESS: ROCKWELL "C"SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST. BEADING	240READING	TOTAL	AVERAGE
		31	34	65	
BOIT	2	34	35	69	$\neg$
BOLT	3	32	3 <b>3</b>	- 65	7/
				199	<i>3</i> 3
		28	27	55	
A /	2	27	27	5 <b>4</b>	$1 \times$
NUT	3	29	29	5 <b>8</b>	
				167	28
SPACER	2-Bc	64	65	129	65
SPACER	2-8	65	65	130	65

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2º0 READING	() AVERAGE	PAVE. X 1.33
		21	24		
ROLT.	2	24	25		
BOLT	· 3	18	20		
				22	29.3
		15	20		
NI.	. 2	22	25	$\rightarrow$	
NUT	3	18	16		
·				19.3	25.7
SPACER			RM. S 20.1		
SPACER	2-8	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº. <u>E-E</u> AN STO. Nº. <u>AN 7C-36</u> NUT Nº AN 363 C-720 SPACER Nº 2 Cc & 2 C

HAPPNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

					7-12-7
IJEM.	SPEC. Nº	IST PEADING	2MPREADING	TOTAL	AVERAGE
		34	35	69	
BOIT	2	3 <b>5</b>	36	7/	
BOLT	3	34	35	69	
				7/	35
	1	28	28	56	
N 1	2	25	26	5/	
NUT	5	28	27	5 <b>5</b>	
				162	27
SPACER	2-C	63	64	127	64
SPACER	2-60	64	65	129	65

SURFACE FINISH (R.M.S.)

ITEM	SPECNO	15 READING	2º0 READING	AVERAGE	AVE. x 133
		35	45		
Box	2	19	14	23.6 /4.5	
BOLT	3	13	16		
				23.6	31.4
		9	//		
N/	2	20	17	$\times$	
NUT	3	14	16		
				14.5	19.3
SPACER				SEE PAGE	
SPACER	2-Cc	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

\_\_\_\_\_SERIES BOLT

CODE Nº F-F

AN STD. Nº AN 8C- 37

NUT Nº AN 363 C-820

SPACER Nº 2 DC 620

HARDNESS:	ROCK	WELL "C"	SCALE, 15	OKG. Lo	PAD
IJEM.	SPEC. No	IST. READING	240 READING	TOTAL	AVERAGE
	١	29	30	59	
BOLT	2	3/	32	63	$\rceil \times  $
COLI	3	3/	31	62	
-				184	3/
	1				
1					
1 11.	2				
NuT	2	3/	33	64	
	2 5	3/	33	6 <b>4</b>	32
NUT	2 3 2-0c	3/	33		32

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	2 NO READING	AVERAGE	PAVE. x 1.33
		13	17		
Boir	2	12	13		
BOLT	3	16	16		
				14.5	19.3
	1				
NI	2			$\times$	
NUT	3	20	16		
				18	23.9
SPACER	2-0c	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	2-0	()AVERAGE	P.M.S20.1	SEE PAGE	

NOTE:

(1) READING CORRECTED TO PROFILOMETER CALIBRATION.

#### HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº: G-G

AN STD. Nº: AN 9C-37

NUT Nº AN 363 C-918 SPACER Nº 17 € 18

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

MEDITOR				_~~~	~~~ <u>~</u>
ITEM.	SPEC. No	IST PEADING	24PREADING	TOTAL	AVERAGE
	١	31	30	61	
BOLT	2	31	32	63	$\neg$
BOLT	-3	30	3/	61	
	·			63	31
	l	23	25	48	
λ1	2	27	25	52	7 ×
NUT	3	24	27	51	1/ \
				151	25
SPACER	17	54	57	111	56
SPACER	18	54	61	115	58

SURFACE FINISH (R.M.S.)

ITEM	SPECNO	15 READING	200 READING	AVERAGE	PAVE. x 1.33
		23	26		
BOLT	2	22	25		
1000	3	15	21		
	·			22	29.3
	1	18	20		
NUT	2	23	17	$\rightarrow$	
1701	3	17	16		
	1 18 20 2 17	24.6			
SPACER	17	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	18	()AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

### -DATA SHEET

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE No. H-H

AN STO. Nº. AN 10C-37

NUT Nº AN 363C-1018

SPACER Nº 19 6 20

HAPDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

10,700	1,44 414				
ITEM.	SPEC. No	IST. READING	240 READING	TOTAL	AVERAGE
		35	35	70	
BA T	2	34	35	69	
BOLT	3	35	35	70	
				209	35
	1	26	26	52	
N/	2	23	23	46	
NUT	3	19	19	38	
				136	23
SPACER	19	62	61	123	62
SPACER	20	<i>5</i> 7	58	115	58

SURFACE FINISH (R.M.S.)

ITEM	SPECNO	15 READING	2º0 READING	AVERAGE	AVE. X 1.33
		/2	//		
Bay -	2	10	9	$\sim$	$\sim$
BOLT	3	13	10		
				10.9	14.5
	1	16	/7		
N.L.	2	17	19	70.7	
NUT	3	16	22		
				17.8	23.7
SPACER			RM.S20.1		
SPACER	20	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE No. I-I

AN STO. Nº AN 12C-41

NUT Nº RN 363 C-/216 SPACER Nº 22 € 23

HAPPNESS: ROCKWELL "C"SCALE, 150 Kg. LOAD

PEDIATO.	17000	77666			7-10
ITEM.	SPEC. No	IST. PEADING	240 READING	TOTAL	AVERAGE
	1	<b>3</b> 2	32	64	
BOIT	2	31	30	61	$]$ $\times$
BOLT	3	32	3/	63	
				188	31
		29	29	5 <b>8</b>	
N/1	2	30	30	60	
NUT	3	28	29	57	
				175	29
SPACER	22	61	57	118	59
SPACER	23	60	61	121	61

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	2 ND READING	AVERAGE	PAVE. X 133
		13	/3		
Ba	2	20	15	$\sim$	
BOLT	3	/3	14		
				14.7	19.6
,		14	17		
	2	15	20	$\rightarrow$	
NUT	3	21	22		
	,			18.1	24.1
SPACER	22	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	23	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº J-J

AN STD. Nº AN 14 C-42

NUT Nº AN 310 C - 14 SPACER Nº 25 \$ 26

HAPPUESS: POWELL "C"SCALE 150 KG LOAD

MARDNESS:	KOCK	WELL C	SCALE, 19	CRG. LO	AD
IJEM.	SPEC. No	IST PEADING	240READING	TOTAL	AVERAGE
	1	32	32	64	
BOLF	2	30	34	64	
BOLT	3	30	32	62	7/ 📐
				190	32
	ì	30	31	61	
N / 1	2	31	30	61	
NUT	3	29	29	<i>58</i>	
				180	<i>3</i> 0
SPACER	25	60	59	119	60
SPACER	26	59	59	118	59

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	Ave. x 1.33
	1	21	19		
Box	2	19	21	$\sim$	
BOLT	3	19	20		
				19.8	26.3
		21	33		
Nive	2	27	22	$\times$	
NUT	3	28	27		
				26.3	35
SPACER	25	() AVERAGE	RM.520.1	SEE PAGE	
SPACER	26	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

## DATA SHEET

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE No. K-K

NUT Nº AN 310C-16

AN STO. Nº. AN 16C-42

SPACER Nº 28 6 29

MARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. No	IST PEADING	2NDREADING	TOTAL	AVERAGE
		32	34	66	
ROLT	2	3/	32	63	$7 \times$
BOLT	3	32	32	64	
	·			193	32
	1	23	24	47	
λ. l	2	27	24	51	$\overline{}$
NUT	3	24	23	47	7/ \
,				145	24
SPACER	28	67	67	134	67
SPACER	29	56	57	113	57

SURFACE FINISH (R.M.S.)

ITEM	SPECNO	15 READING	2 ND READING	AVERAGE	PAVE. X 133
		16	16		
BOLT	2	25	18	$\sim$	$\rightarrow$
BOLT	3	24	2/		
				20	26.6
	1	18	16		
NUT	2	12	11	$\rightarrow$	
1701	3	15	23		
				15.9	21.1
SPACER	28	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	29	()AVERAGE	P.M.S20.1	See Page	

NOTE:

(1) READING CORRECTED TO PROFILOMETER CALIBRATION.

. HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE Nº. L-L AN STD. Nº. AN 18C-44 NUT Nº AN 310C-18 SPACER Nº 30 4 31

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

ITEM.	SPEC. Nº	IST. PEADING	2NOREADING	TOTAL	AVERAGE
	١	<i>30</i>	30	60	
ROLF	2	28	31	59	
BOLT	3	<i>32</i>	32	64	
				/83	3/
		20	22	42	
`A /	2	24	21	45	
NUT	3	19.	19	38	
				125	21
SPACER	30	60	64	124	62
SPACER	31	54	58	112	56

SURFACE FINISH (R.M.S.)

ITEM	SPEC.Nº	15 READING	200 READING	AVERAGE	AVE. X 1.33
		10	12		
Bar	2	10	10	$\times$	
BOLT	3	11	21		
				12.3	16.4
		16	11		
NI.	2	15	14	$\times$	
NUT	3	17	13		
				14.3	19
SPACER	30	() AVERAGE	RM.S20.1	SEE PAGE	
SPACER	3/	(I)AVERAGE	P.M.S20.1	SEE PAGE	

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

# DATA SHEET-

HARDNESS & SURFACE FINISH

AN SERIES BOLT

CODE No. M-M

AN STD. Nº AN 20C-45

NUT Nº AN 310C-20 SPACER Nº 32 6 33

HARDNESS: ROCKWELL "C" SCALE, 150 Kg. LOAD

	1 4 4 4 4				70.
IJEM.	SPEC. No	15T. READING	2NDREADING	TOTAL	AVERAGE
	1	26	3/	57	
BOLT	2	25	27	52	
1 2021	3	26	28	54	1/ \
, '				163	27
	1	26	24	50	
NUT	2	28	29	57	
1001	3	28	28	56	1/ \
				163	27
SPACER	32	- 59	· 55	114	57
SPACER	33	59	59	118	59

SURFACE FINISH (P.M.S.)

ITEM	SPEC.Nº	15 READING	2ºDREADING	AVERAGE	AVE. X 1.33
		17	12		
BOLT	2	14	14		
002/	3	15	13		
				14.2	18.9
`	1	14	23		
NUT	2	47	32		
1701	3	40	32		
				31.3	41.6
SPACER		() AVERAGE		SEE PAGE	
SPACER	33	(I)AVERAGE A	P.M.S20.1	SEE PAGE	· · · · · · · · · · · · · · · · · · ·

<sup>(1)</sup> READING CORRECTED TO PROFILOMETER CALIBRATION.

#### APPENDIX III

DATA SHEETS
of
TORQUE TENSION RELATIONSHIPS

SETTLY SHOWING 1 for STATES (CONTROL OF STATES STATES (CONTROL OF STATES STATES (CO.)		Topauro Form Mir		2000 3000 2000	27	25 55 90 27 79 35 53 73 26 79 32 50 73	2 20 45 80 87 (13 5 19 32 50 25 125	7 25 44	10 27	10 27 45 62 93	7 25 44	9 29 53	10 29 45 66	13 36 56 75 101 140	9 29 45 66 90 1	6 16 32 49 71 109 6 14 22 55 90 132	442 1 8 20 34 51 75 116	9 20 32 49 69	77	12 25 40 59 95 1125 140	8 26 44 70 109 118	12 30 45 69 85 120 173	13 35 50 70 89 115	12/	54 85
COURSE LA DATA  COURSE LA DATA	CUBBICATED	Descreto Fram Head	TENSILE STRESS ("IN")	संस्कृत संस्कृत संस्कृत संस्कृत संस्कृत सार्वेक स्कृति हैं। स्कृति सार्वेक संस्कृति सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक सार्वेक	22 39 56 79 96 MVL 19 31 45 60 80 80 80 80 80 80 80 80 80 80 80 80 80	24 7 24 97 55 69 85 500 402 500 47 500 68 85 500 68 600 600 600 600 600 600 600 600 60	5 18 41 56	98	7 28 43 55 74 91	9 24 38 54 71	52 67	39 55 73 92	12 3/	10 27 42 58 76 93 A	38 54 72 98 M	79 31 45 61 78	0 25 39 55 71 90	7 23 37 50 63 72	25.4	8 27 41 60 78 100 129	73 90 1/9	20 30	4 1/ 27 40 55 66 83 104	19 25 40 58 73 91 117	THE WHICH CHARLE STREET LIVE - 2381 MINOR C. 20 36 38 46 18 83 104 MALL MALL C. TST ON DELL'S DESCRIPTION OF THE PRESUNCT TRUE . REPRESENCE THE PROBLEM OF THE PRESUNCT TRUE . REPRESENCE THE PROBLEM OF
V <u>er</u> <u>B</u> 5:0 5:0 88, 51 Mante, Cat. Coep, Unlow, N.J.	LUBRICATED	TOROURD FROM NUT	FUSILE STRESS (#/w.2)	10 000 3000 (20.00) (10.00) (10.00) (10.00) (10.00) (10.00)	13     38     70     105     152       21     56     94     /41     198       27     78     126     189     265	77 (28	13 38 30 105 152	73 /32 202	35 141 215 274 365	352 337	4/ 96 7.33	3V 71 191 309 375 467 507	60 /66 246 321 395	376	38 95	73 /89 282 366 42/	7 /6/ 246 325	65 164 247 325		100 147 197	30 77 205 21 dos 400 656 600	68 170 261 837 428 516	53/	311	TO WHICH CANSED RUPLYEE OF TEST ON BOLT IN DIS BIE WING IN BOLT IN DIS BIE WING IN WORTH WING IN SANDIDONG
Test Cell   Second	A Now Luis	Toeover Few Hear	TELISILE STRESS ("MIS)	19 1000 3000 59.000 79.000 99.000 110.000 140.	25 57 94 132 150 20 57 94 132 150	54 21 52 AVE: 23 56 MARK: 26 59	14 47 111 163 201 2	37 /04 /54 200	54 50 119 153 204	1 Mar. 32 1/14 163 263 244 Mar. 32 1/14 163 205 244	14 54 /32 /86 (2)	34 41 (19 175 34 41 (19 175	51, 120 170	Mas. 54 132 186 223 May 41 117 169 219	IH TEST DISCONTINUED DUE	46 125 174	5H 47 1/7 170	Aut. 48 127 178	Marx 46 117 170	24 E.S. JOSCHNINGED BUE TO RUPTURED JESTS L.	50 /33 /9/	W 54 129 172 218 258 E	ANS 54 130 184 225 265	Mar. 55	L Now LOADMELTS: 2, Best Through The Condition Souls Shift weeke making to the values less than the CONDMELTS: 2, Best The souls of the bouns shouther to the That, District Souls Shift S

WADC TR 57-330

SKETCH SHOWING HERD  FUEL SEMBRACE HAT HIERAND  FORE STREET SHOWING BLOCK  (BOCKWELL V. S. SCALE GO)	LUBRICATED	TUR WAST CHURSOT	TENSUE STRESS ("/W.")	10,000 30,000 60,000 10,000 30,000 60,000	24.2 10	27 47		50 73 102 137	12 37 65 95 123	14 95 63 90 123	20 50 73	2 06 07	8 23 48 70 100	29 50 77 108	9 25 49 74 705	8 21 #3	200 /3 35 62 89 /10 /40	92 68 90 128	504 15 95 72 95 122 197	13 38 65 89 121	117. 20	24. 5 24 50 72 110 142	32,	341 8 25 50	0 45 70 102 135 160	2 20 40 72
TEST DATA  COURSE LE BEST DATA  NOTE: NOTE	Devota lensus Singus Repeated	TOROUED FROM HEAD		A 1 1000 30,000 00,0000	M44,612 30 52 78 705 1.37 34,41,5 28 50 77 105 728 34,41,5 35 40 02 7.3 6.0	66 99 131	19 43 66	244 13 37 65 82 105 127	25 78 105 145	40 58 87 119 1	12 55 78 105 145	48 73 97	34.2 10 35 50 75 105 127	28 55 77 103	13 35 63 77 108	5 25 48 73 97	24.4 8 37 70 92 1.10 132	97 70 100 138	17 36 57 84 116 1	70 100	142 L 5 25 53 7	246 7 32 67 85 123 198	4444 10 25 50 75 90 123 153	542 4 30 53 87 126 151	10 29 56 82 113 137 177 178 187 189 187 177 178 189 189 189 189 189 189 189 189 189 18	CONTINUE SUBSEQUENT LUBERCATIONS
TEST CELL - NS: TOWNSON - 78 TOWNSON - 78 TOWNSON - 78 TOWNSON - 78 TEST THEST ELASTE SOP NOT CORP. UNION, N. J. P. II.	BEICATED	TORQUEO FROM NUT	(*) TENSILE STRESS (*/1,2)	335	20 59 /39 224 339 946 516 30 50 /29 230 322 92 976	40 40 123 223 327 447 562 40 45 72 216 33 472 565 40 72 216 33 472 565	37 100 180		85 227 341 447 847 84 212 326 431	85 212 340 474 625	80 178 277 365		104 2.90 932 554 637	105 267 492 645 692	165 291 409 534 671	310 400 475	128 318 464 615 714	40 (20. 3/7 48/, 622 77/, 017	115 336 522 698 815	MM. 128 336 512 698 815 917 MM. 95 320 321 436 500	100 225 320 410 467	489 640 763 827	div.	54 128 396 566 741 849 919		1, Bost 1, 17, socces from Entrances of tockounks tock at END or 200 Bacquines, Test on the 21 Discontinues. 2, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18
6 APRIL 1956  B. She-34 UNF-35  V. CR CRAT — NS. MONG-570 MTTD 89	Non LUBRICATED	Toequeo Feam HEAO	7	10,000 30,000 52,000 74,000 30,000 110	7 /45 232 328 7 /31 /99 299 7 /30 /92 249	74 100 218 283 64 134 199 262 66 128 207 274	60 (00 (92 349	100 230 311 392 4670)	92 225 352	910 990	1-#-	ZH " ZET DISCONTANDED DUE 19 INTERNAL KUMVER OF PIEMD	95 240 336 444	105 250 389	105 255 365 484	240 336 444	3H Town Challent Child as without a	1	011		<i>M</i>	新		97 273 389 487	Mar. 97 273 389 487 562 567 May 97 273 389 487 562 567	COMMMERITS: 1, BOLT II (1) 1 6.24 SOCKET MAD RUTURD OF TREGOUNES 1 3, KUNG OF LUBERATED TOKRUINGS ARE MAKED (1,5) PARE BUCKES WERE SANDED AT THE BULD OF TH
Dane Size Scene	WAE		a/Y <b>5</b> 71	57-33	rinoseg	7 7	\$   \$		فَحده		.1. 1	±im 	_[_	**************************************	1 1	1	brin	Ш			Ш		200	L.	ш	8

WADC TR 57-330

6 Head Headeway Places			STRESS (#/WZ)	निकार जिल्ला क्रिक्ट निकार निकार निकार निकार निकार	100 275	208	+	218 285	217 279 250 310	230 295	155 300 150 250 235 235	255 263 255 300 190 250	200 270 200 270 200 265 200 265 200 275	2/9	245 300	<del>                                      </del>	240 300 190 250	Process
SKETH SHOWING HORD FLUET (LEGATIVE IN HORDEND STEEL SPRING SHORY STEEL SPRING SHORY	,	TOROUED FROM NUT	TENSILE STR.	क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ क्रांस्थ		10 115	65 45 50 90	+-	25 85 145 164 26 50 90 140	60 80 /	9000	22 76 120 173 40 100 165 205 25 60 80 130	35         85         130         200           25         50         90         140           35         65         1/5         170           35         40         1/5         175           30         70         1/5         175	20 115 85 130	30 30	50 35 1	34 81 (22 177 500 10 165 215 20 50 80 135	
- 66. — — — — — — — — — — — — — — — — — —	CUBRICATED		(#/WE)	मा क्रिक्ट में क्रिक में केर में क्रिक्ट में क्रिक में क्रिक्ट में क्रिक्ट में क्रिक में क्रि	34.5	270 SAL 285 ALE 315 NAW.	215 104	250	265 Ave.	285	2.80 30.5 30.5 40.21 2.90 50.2	240 247 Mes. 160 325 Mes. 230 280 Min.	215- 275- 275- 285- 285- 275- 275- 275- 275- 275- 275- 275- 27	Mus.	350 470 1142	305 405 SWL	Name.	T OF HEAD BENEWG SURFACES
(b) 2809 Note: HOppmass (1)	Deviore Teisue St	TOROUEO FROM HEAD	TENSILE STRESS	acota contract	70 70 70	1/10 165	80 125 175	70 1/8 155 5	20 /25 /55 70 //0 /50	95	98 /45 /45 2	100 155 205	35 /50 200 60 /25 /75 90 /25 /85 75 /25 /80	90 150 200	100 205	85 155 210	110 164 212	SOCKET HERD ET TOKODIE LIKENET HIS STOLEDING. INIS OF EKY TOKODIE SOCKETY, WERKENDON AND SUBSCONENT LUBBERGIENS OF ANT OR HEAD BENEWIG SURFACES. WERK CANDITIONS ONLY DIG TO SCHREMG.
7.557 DATA Courden Nº Nº 38 (UA) 2609 P. 1277				O Hacena (1000)		4 5 5			12 20	$\geq$	77.77	2 2		1320 Ann. 29 1320 Ann. 40 825 Anu. 92	5 1000 142 KS 5 1975 242 40	1325 444	15 1475 MAR. 55 15 1000 MIL. 40	LEGATOR STOCKLONG.
		IEO FROM NUT	TENSILE STRESS (#/w2)	59,000 79,000 99,000 119,000 1	255 360 475 590 445 665 820 1000 325 470 610 800 445 605 790 955	345 530 695 830 363 536 678 835 445 665 820 1000 855 360 470 590	845 /025	830 975	875 1045 11 46a 580	089	865 00/5	089 355	780 994, 1/80 925 780 994, 1/80 1220 762 980 1/80 120 705 890 1/50	580 1180 580 710	780 10/0 1/65 1305 785 980 11/0 1230	200 1045	445 1010 165 18 445 585 710 8	SOCKET HERD BY TOKODIE LIKONOM ING OF ERKY TOKODING FOR MITTAL LUBRICATION IF BY CONDITIONS ALLY DUG TO SCARRING.
Test Ceut — Nos. Tessen — 174 72 Compressen— 5 B Amerent But Gom, Et Monte Ga. Eustic Stop Mit Gom, Li Monte (Au.	Now LUBRICATED	Takon	74	ocace soor	50 70 1/0, 295 80 205 95 255	10 208 10 208 10 208 10 208 10 208	450	950	120 465	ZN 235 530	225 990 195 975 198 459		250 550 230 550 250 495 210 5/5	Man. 250 550 Man. 125 3.05	M 130 300 2U 205 585 3U 225 565	50 220 530 Ave: 219 408	MAN. 275 565 MIN. 130 300 PUTURED BY TORBYING TOOL BET	POINT TO AYOLD RUPLIEGE OF WITH AN "L" AT THE BEGINN PROQUING OF CANN SPECMEN PORTH
MFT0 98	Nav Lui	Toequeo Few Heno	STRESS ("/w")	37,000 59,000 79,000 90,000 111,000 11	680	500 625 735 / 522 658 790 570 715 850 478 600 735	760 950 1025			830 970 1/00	920		920 920 925	975	820 960 1110 maco 810 935 1050 m 775 925 1030 m	805 910 1010 (1) 815 935 1060 (1) 805 933 1052 93887	820 960 1110 775 910 1010 DOLT 1-H SPECIMEN SOCKET MEDI	3. Both 34 to 54 work way tokoved to victs have to hear to those resplice of 3. Ewis of tubblents resolutes he maked win in ''n the begin it. Ships begin in the second for the ships have ships in the second here.
4 4 COUT - MS ;		Toesure		10,000	\$5 215 335 95 260 400 700 255 400	42 450 570 48 451 785 725 475 420 85 415 335	/80 430 595 /95 440 630 /95 445 625	195 475 650 195 425 600 198 443 620	180 425 595	205 485 670	225 480 660 185 465 650 200 421 656	185 485 670 185 185 630.	215 480 695 220 475 650 225 475 650 205 470 655	225 480 195	210 475 660	225 985 658 200 975 660 209 474 652	3 5	COMMINENTS: 2. BOITS 2H TO SH. 3. FUNS OF LUBBI. 4. SPACER BLOCK
•	WAD		N 47	200	-	Server S		3 3 W	11.	Ш	1000	Harry	TO SE SE SE	ZWIND D		# 13 W	S	Committee

Compact Float   Page    Served Schwarz Head.  Served Schwarz Head.  Final Cleanure Michaepener  Free Schwarz C. Scale 60)	CATED	TORONE FROM NUT		STATE OF	99 V (42-2) (42-	125 190 270 105 150 220 95 164 237 125 190 270	20 20 20 20 20 20 20 20 20 20 20 20 20 2	28 /00 /75 296 325 1 25 75 /90 215 280 30 92 /66 238 325	140 205 250 150 150 150 150 150 150 150 150 150 1	45 (12 140 150 350 45 (15 10 20 305 365 135 (15 10 20 305 365	45 125 200 275 360	Mx 40 130 220 302 380 495  344 50 135 220 302 380 485  444 55 135 265 275 375 345 470  444 55 135 213 28 35 471  478 50 140 220 220 370 470	125 230 330 435 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	41-35 75 195 215 41-40 10 185 260 41-30 73 195 220	435 315 7 716 5 74 70 M D/ 170 M S	
Contract   Contract	NOTE: (IIII)	URIOTA (ENSILE STATES REVIEW)  LUBRICATED		(*//NE)	A COST SCORE SCORE SCORE SCORE COSTS COSTS COSTS	11 (14.4)	20 15 195 205 205 205 205 205 205 205 205 205 20	30 85 170 245 305 25 85 165 235 315 20 82 147 315 160	20 95 170 210 310 20 91 165 232 309	20	35 //5 216 270 380	30 100 135 225 280	25 (30 245 350 920 45 (40 240 350 925 35 (15 220 55 35 30 (17 195 215 315 30 (17 25 215 316 50 (196 218 319 50 (196 248 319	35 105 190 245 325 345 40 135 240 350 930 520 45 145 245 320 422 522	25 90 175 225 300 395 195 125 230 290 355 94 29 123 222 294 372 441	Apper 35 90 125 350 1550 1550 1550 1550 1550 1550 1550
Cocal   1956   Coca		RICATED	MOSY C	J' TENSILE STRESS	जिल्हा जिल्हा कार्य जिल्हा कार्य जीता के कार्य के कार्य के कार्य के कार्य कार्		255 5:00 164 60.5 10.0 257 5:00 164 60.5 10.85 257 5:00 165 10.5 10.5 1.55 5:00 165 10.5 1.55 7:00 45.0 60.5 77.0	265 550 775 950 125 255 650 940 255 1955 865 715 1000 1355 1975	315 620 570 1/20 1/320 245 740 1/25 1565 1600 315 65 744 1/81 1/35 365 740 1085 1865	245 550 775 950 1125   125   125   125   125   125   125   1270	715 130 1100 1350 1555 1305 635 925 235 1915 1313 711 1061 1285 1515	425 830 1285 1450 190 775 635 880 1090 1270	350 125 125 1315 1545 1315 1545 1315 135 135 135 135 135 135 135 135 1	340 1200 1000 1300 1443 1705 340 1200 1000 1305 1555 1775 3713 1765 1665 1330 1560 1750	44/ 315 600 //35 //950 //750 //455 54/ 345 600 //35 //950 //950 //950 54/ 340 600 //35 //950 //950 //950 4400, 356 600 //350 //950 //950 //250 4400, 356 600 //350 //950 //950 //250	530 1190 1450 1675 HEAD RUPTURE BY TOOL WATH THE
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+ 3	LUBRICATED		<u></u>	8.8	25			<u>T</u>	[ <b>Q</b> ]	NUM.		<u>:</u>			1	17	ŠĮ.	$\vdash$	Ц		4	<u>4 8</u>	Ž		<u></u>		$\frac{\perp}{}$	2
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NOTE:		TOROUEO FROM HEAD	TENSILE STRESS (*/IN!)	0000 2000 0000 0000 0000 0000 0000 000	THENE TORUE TORNE THENE THENE TORNE (MI-9) (MI-9) (MI-9) (MI-9)	332	275	275	292	332	380	300	370	3/0	335	380	300	480		-+	355	345	280	470	330	-†-	322 385	✝
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TEST.			Ţ.	Morence. MO,000	No.		$\times$	7				$\geq$	×						×	<		Ì			>	<u></u>	<u>/</u>	
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		M MC	RESS	accia	200	960	+-1	15/5	194	1515	1270	1725	1585	1855	1632	1855	1270	206/	5/2/	T.1	1915	1782		52.57	1950	1870	2100	
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SKATU SABUM HAD COURTESSIE IN HADOND STATE SCHOOL BLOCK (SOLKHRIL TO STONE GO)	77ED	Towners from Mrs	Jan June 1	THE STATE THE ST	1280 700 320 1160	740 132020802880 800 146020602660 812 1404 2054 2704 1160 1790 2340 2880	344, 200 560 160 180 200 340 340 340 340 340 340 340 340 340 3	18304-200 740 1320 19492549 3080 1844-284-780 1400 3028 1471 3271 1844-350 1080 1480 340 340 4000 1844-350 540 1060 600 340 3640	10/220 60012001720224012700 20/2360 1100 1680 2340 3000 3800 30/2340 940 1520210026403100 (8) 30/2 4 601 6002180 220012340 (8) 30/2 4 601 60021500 200012540 3180 30/2 976 976 976 9764 4448 3490	13222	
CONTRACT LASTA (18.00) NOTE: 10 Procuments (18.00) (18.00)		TOERVED FROM HEAD	TENEVIE STORES (#/1.18)	1000 90,000 (1,000) (1,000) (1,000)		4 80 900   4 80 2 40 2 80 35 8	2340 3060 3860 2220 3220 3980 2300 3140 3800 2000 2760 3560	360		1860   3460   3160	280   280   280   288   374   188
. 60 A	WILL ALSO, LITERIA CAN. J	TOROURD FROM NUT	TENSILE STRESS (#/1/12)	(1.11) (1		1040 17602260 2296 3608 4751 3100 4600 5940 1040 1760 2360		380 6600 380 6600 1340 2940		1 19911	200 774 9 9 10 0 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2
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DATE 21 FEBRUREY 1951 SIZES 1, 18-10 UNIT- SA CONDITIONS————————————————————————————————————	
SUREW OR BOLT MS 20018-SM MED BY AIRCRAFT BOLT CORP. EL MONTE, CRI.  STREE SPREIMS BLOCK  CONTRACT UP HF 33 (616) 2808  NOTE:  (NOT FOR BOLT MARKED (A) PRINCE DY LOCKHEED MIRCONT CORP., GLIEBANK, CRI.) 2  NON LUBRICATED  NON LUBRICATED  LUBRICATED	
CONTRACT UNIT FOR SOLT MARCO (1) PROBLEM COND. BUREAUX, CAL) & P. 1221 Fishers, In Programius.  (NOT FOR SOLT MARCO (1) PROBLEM COND. BUREAUX, CAL) & DEMOTE TOOMS. BUREAUX, CAL) & DEMOTE TOOMS. BUREAUX, CAL) & LUBRICATED	
NUT 2.5 CB - 148 MED. ST EXERCE ON OF STOP PRESSED STREEL CO., JOHNSTOWN, PR.  (NUT FOR BOLT MARKED (1)) PURMSHED BY LOCKHAED PURCHAED PUR	
Non Lubricated Lubricated	
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COMMENTS:

(1) BOLTS TORQUED FROM THE MED IN THE DET CONDITION WERE TORQUED TO JO, OND OR SIGNOD PS I ONLY TO PREMENT RUPTURE OF THE SOCKET A HEX, WARNEY AT VALUES OF TORQUED ABOVE 8000 IN-L [3] STATE CHARLES MADED BEFORE EACH ZUN FUR. BOTH LUBRITATED AND DAY CONDITIONS DUE TO SOMETHINE TO SOMETHINE SOF TORQUED FOR AN ARE MARKED WITH AND "Z" AT THE BESIMING OF THE RUN TO INDICATE INTIAL CUBRITATION AND SUBSECUENT LUBRITATIONS OF INT OR HEAD BEARING SURFACES.

SLATIC SLAMING HASO  THE CONTROL OF GRACIOUS  STATE STATES THE COLONIES  (POLENIEL C') STATE (CO)	CATED Transier From Mer	TEST TO THE PARTY OF THE PARTY	36 000 02 0	344 160 800 1800 2900 40.25 5.40 344 160 800 1800 2900 40.25 5.40 344 160 800 1900 2900 40.25 5.40 344 160 800 1900 2000 40.25 5.40 344 160 800 1900 2000 2000 2720 345 200 100 100 2000 2720 345 200 100 100 2000 2720 350 200 100 100 2000 2000	150 800 1900 4 150 800 100 4	244, 120 820 2100 3460 4840 6180  344, 200 620 2280 3820 5260 6300  344, 160 1000 200 200 300 4400 5900  350, 240 880 1890 260 3140 5900  340, 240 980 180 200 200 310 310 300	120 800   140 960   150 1080   150 1080   150 1080   150 120   1	7 2 2 2 2	748. 240 1500 2400 3800 3240 4400 100 100 100 100 100 100 100 100	780 19002960 42805700	160 1020 2000 3340 204 1096 2208 3408	Han. 120 120 1880 4960 3860 1360 1360 1360 1360 1360 1360 1360 13
19077 18 18 35 (46) 2808 Nord: 1721 George Green Reservants 1800 George Green Reservants	TOTO LEGIC HEAD HEAD	TENSILE STORES (*/1,1)	13,000 39,000 50,000 20,000 92,000 110,000 110,000 100	MAC	740 7520 1340 3480 140 900 1760 3460	344 160 180 1720 2880 4180 5500 344 180 860 1740 2880 4180 5500 [10 444 220 1840 2040 3101 4300 5000 [5)544 200 1160 2080 3200 4500 5700 [6)544 200 1160 2080 3200 4500 5700 [6]544 200 1160 2080 3200 4500 5700 [6]544 2080 3200 4500 5700		160 (90 7%) 200 160 (90 7%) 200 17-20 (200 220 320) 17-20 (200 2100 330) 17-240 (200 2100 330) 17-240 (200 2100 330) 17-240 (200 2100 330)	920 3200 3260 920 1900 3260 1080 2 240 3460	244, 220, 000 22003580 5000 6240 7860 344, 160 900 20003220 4400 5520 7340 (M444, 260 7260 2320 3500 4640 5840 7580	2883	MINU. 150 900 2000 31.20 4400 5520 70400 0000 0000 0000 0000 0000 0000 0
7 (1841) √ (1841)	TORQUED FROM NUT	J TENSILE STRESS (#/N.3)	1 2000 3000 3000 CM. 19	97601 171001 108601 5700 7580	100. 1500 5540 8300 1070 13080 17080 5700 2700 2700 13080 13	2200 5240 8140 10760 13.60 12.00 17.00 13.60 12.00 17.00 5160 6740 8420 12.00 12.60		\$500.0   \$450.0   \$750.0   \$1350.0   \$1950.0	1400 5500 7660 9800 11660 13380 2000 6700 9960 13120 15840 19200	30. 2880 7420 13100 168401 3700223802500 30. 2880 7420 10400 14500 17200 19400 22100 (0040, 2840 5800 8300 10740 12880 14620 16900	28/2 6060 896011900 146601 28/2 7076 10144 13420 6086 3820 9400 13100 16840 19700	FOLGO THE WAS ALLOW TO THE WAY TO SELVEN THE WAY TO SELVE THE WAY TO SELVE THE WEST OF THE WEST OF THE WEST OF THE WAY TO SELVE THE WAY TO SELVE THE WEST OF THE W
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Sterey Stelling Head	OZU.	TORQUED FROM NUT	TENSILE STRESS (") (")	(1,000 30,000 50,000 70,000 90,000 110,000 910 810 810 810 810 810 810 810 810 810 8	Mr. (3500 1600 3000) 5020 7080 9360	600 1740 3100 4900	460 1580 2600 3700 5020 460 1/80 2300 3580 5060	2300 3580	480 1600 3120 5020 6940	304 480 1560 3120 5040 6920 8800	680 1420 2380 3600 4880	1240 2360 3860 5300	+	1240 2360 3600 4880	244, 500 1600 3300 5060 6800 BEECO	1760 3560 5380	600 1400 2500 3760 5380	5460 7	0865 0956	1 600 1700 3160 4900 6700	1560 2.900 4880 6600	600 1400	14 20 1300 2600 4100 5580	Max. 600 1200 2540 3400 3400 3060	480 1580 3040 4	400 1500 3060 4900 6520	1640 3300 5440 7220 8940	7 60 7 600 600 4000	484 1552 2	Max 560 1600 3300 5440 7320 8440 11600 Max. 400 1440 2600 4000 5540 7320 9860	
5.7 D4779 	LUBRICATED	TOEQUED FROM HEAD	TENSILE STRESS (*/W.)	(2.11) (2	2780 42.00 6160	2440 40 00 5 560 7 440	2500 3620 5120 6600	1000. 500 1600 3780 4200 6160 8120 M	1,520 1500 2900 4400 6100 7840	342, 260, 1300, 2700, 4180, 5800, 7480	4 80 1500 2 689 4040 5600 7200	42 4 60 1460 2620 3960 5300 6800	Mrs. 436 1440 2672 4120 5684 7316 A	260 1240 2460 3960 5300 6800	74.2 420 15.80 3000 4600 6240 7900	1300 2680 4300	-4 80 1560 2940 4520 6020 7600	7556	MAN. 520 1580 3000 4600 6240 7900 A	480 7600 300 0 4720 6500 8100	1520 3020 4700 6100	520 1560 2840 4220 5820 7280	12 1500 1560 2880 4300 5920 7600	1996. 520 1600 3020 4720 5030 8100 1997. 520 1600 3020 4720 5820 8100	1600 3060 4620 6220 7950 10980	4201500 3100 4620 6260	1300 2800 4260 5820 7300 9960	8) 447. 520 (500 2900 4 160 5880 7400 9880	Aur. 540 1620 2 900 4 600 3820 1260 5500	1000 540 1620 3100 4620 6260 8020 10980 10010 10010 10980	LET & HEX WRENCH AT MALUES OF TORD
51	Nav Lusercareu	Tokoueo Fean Nut	J TENSILE STRESS (#/w.a)		W 1860 5480 9740 13780	1600 3400 5600 3000	■ 1 400 3 800 4 800 1 200 1 4 800 0 1 4 800 0 1 4 800 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1960 5480, 9740 1:1780 18.	2620 7700 11540 15580 190002	30 3 400 5600 8600 1400 1400 14000	3000 7000/10800/13600//000	1200	1405 2244 5540 8628 1396 14640 17236	1200 3400 5200 7	ZN 230015 20 800 15860 19360 22560	12800, 7400 [10800   15000   19200	3600 8000 12000 15600 19000	Ave 1688 6584 9976 13292 1652 19592		13800 9200 13800 18000 218	0000 0000	3200 1200	(B) 50 1 800 4 40 0 700 0 9800 12000 14000	3800 9200	3600 8800	3000 7000 11000 15000	3000 8400 13800 19800 24200	9200 13600 17600 21000	3000 7640 11800 1	1800 9200 13800 19800 24200 1800 4800 7200 10000 1200	O CHENGTON WERE TONDED TO SOOD AS OMY TO PREFERT PRIVILE OF THE SOCK CHENNG. FOR SOFT FOR SOFT TO SOREING.
DATE 21 MARKEL 1957 5,226		K TORQUED FROM HEAD	FUSILE STRESS (*/W.)	A TOWN 33000 5000 TOWN 1000 5000 19,0	14 A	1700 5320	15(6) 17(6)	MAK. 1800 5320	14 2080	34 3000, 7220,112000)	(B) 4:4 2960	H5(8)	N Mex 3760	MIL 2080		34 3000 7 980 18000	3700	(0) 37 4 0 BO	9) NAME 4080 9920 14600	11/ 3400 8	24 3420 8300	(8) 44 3620 9220 13580 11)	(B) 5H 4040	1 100 4 10 10 10 10 10 10 10 10 10 10 10 10 10	40209	KH 3460		(B) 4000 9580	12 Apr 3668 9056 14512	- 1	(1) BOUTS NEWITS: (2) 5PACE

WADC TR 57-330

Seeth Shawing Head  Seeth Shawing Head  Some Spacing Black  Some Spacing Black  Some Spacing Black  Some Spacing Black  Some Spacing Some Some Spacing Some Spacing Sp	LUBRICATED	TORRUED FROM NUT	TENSUE STRESS (#//.1)	A 181	24 00 4 4 00 4 4 00 0	1600 3200 4600 6600 660 2000 3960 6260	Auch 680 2100 3360 6160 8760 1360 Max 1600 3300 4344 6534 6540 11331	2000 3960 6160 8740	20/2 1800 2200 3000 4800 7400 10000	2200 4200	Aux. 840 2240 4004 6104 857 1100			344, 400 1600 3600 5400 8200 1000	300 2300 4320 6 940 9020 11240	800 2300 4208 6328	111/2 1600 3000 5400 7500 9600	2 600 4 800	680 2260 4440	된다	MAN. 800 2600 4800 6900 9360 11940	200 1000 4400 6800 8800 11000	3/1/ 600 2000	40C-780 2400 4420	14. 616 2000 4384 6728 8972 14. 800 2600 4800 6840 9400	nu. 400 1000 4100 6600 8	1
16-57 DATA COURSELLY IF 33 (46) 2809 LONE: 10 Three mines (17) Three mines	1807	Toeques Fenn Heas	TENSILE STREESS (*/N.º)	Cos 05 000 18 00001	740 2200 3860	800 2200 3820 5820 780 2100 3620 5800	2 5 40 2 100 7/2 4020 800 2300	1144 1000 2700 4340 6 200 842010 600	2340 4100	5880 8240	732 2284 3976	260	244, 640 2 100 4500 6500 8200 10500	4400	2300 4400 6440	2560 4500 6560 8940	900 2560 4400	3940 6200	740 2400 4460 6860	2348 4308 6516 88	War. 740 2180 3940 6200 8600 10940	24%	344 740 2300 4500 6700 9200 11740	SH2 700 2200 4140 6540 9040 11660	April 146 226 4328 500 500 1050 1050 1460 1000 1000 1000 1000 1000 1000 100	MAN. 700 2140 4060 6200 8700 10900 AND SOCKET AND HER WEENCH AT VALUES OF TOROUG ABOVE 26,0	TOW AND SUBSEQUENT WERECATIONS OF NAT OR HEAD BENKING SUFFACES
S. S. S. S. S. S. S. S. S. S. S. S. S. S	अराटमार्ट	TORQUED FROM NUT	MIENSILE STRESS (#/1/1/2)	THE PROPERTY CHAIN CHAIN CHAIN CHAIN (MAN)	3400	2000 6600 11600 16400 1800 4200 7600 11400	1640 5000 16 600 1500 15000 2000 6600 11600 16400 21000	1600 4000	30 3000 8800 13000 14400 25600	50 3 4 00 8 6 00 1 2 4 00 1 BOOK 7 2 BOOK	3400 8800	4000	3800 86001	44 2 600 6400 3400 12200 15400 18400	AVE 3160 8040 13 400 16500 2 1600 2 6 6 0 0 3 1000	MAX 44000 10400 16200 21600 24600 31000	10 1/800 5000 7200 10600 13600 16600	30 4800 12600 10200 2 5000 20600 28600	0099	19.55 3 4 40 9 200 14 040 14 16 10 2 2 900 3 2 40 0	M 2000 5000 6	20 4200 11000 1	30 5400 14000 21000 26800 3 2000 3 6600 4 2600		Ane: 3760 9850 18800 19760 24000 27960 33400 AND AND AND AND AND AND AND AND AND AND	FINE THE THORY SECOND SECOND (1900) (1904) (1904) (1904) (1905) (1906) (	177 AN 17.14 THE BEGINNING OF THE RIN TO WOLGHE WITH LUBRICA. FIVE TREQUEST. TO THE WILLE COULD BE RIN WITHOUT HEND RUBRIE. THE
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WADC TR 57-330

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	TOROVED FROM HEAD	TENSILE STREESS (*/in.e)		1 200	12 1000 2800 5400 7800 10800 14000 14000 1200 14000 14000 14000 1400 1200 14000 1400 11200 14600 1400 1400 1400 1400 1400 1400 1	1000, 4800, 5800, 5600, 6600,	1,000 3600 6000 9400 12400 1 1080 3480 6360 9440 12760 1 1400 3800 7400 10600 14600 1 1000 3000 6000 8800 1	1000  3 qua   1400  1600  1400  1   1401  4000  6400  9800  13200  1   1000  3400  6400  9600  13400  1   1000  3400  6600  9600  13400  1   1000  3400  6760  9700  13800  1		1/1/2   1.200   3800   2620   4920   13800   16400   3800   16400   3800   16400   3800   16400   3800	U. 100 320 (120 920 1600) 1500 (1600) IND SOCKET NID NEW WIEWES OF TORBOLE DESCRIPTIONS OF WIT OR HEND BRANKING
SEICATED	TORQUED FROM NUT	J TENSILE STRESS (#//us)	1 1 2 2000 34,000 34,000 34,000 94,000 110,000	4200,1/600,19600,25000,25000 4400,12400,20600,2740033400 44400,10800,15000,1940022200	4 400	- 7100   10700   1900   19400   19600	5 600 12000 5760 13000 6800 16000 5000 11000	6 4 00 16000 6 4 00 12 400 5 4 0 12 400 7 2 0 0 15 00 6 1600 1760 8 1600 1800	200   120		
	TORQUED FROM HEAD	JENSILE STRESS (*/W.)	000 10 000 10 10 000 10 10 10 10 10 10 1	74 4600 11400 214 6600 14000 34 7000 16000 411 6400 14800	54 6000 4000 1000 14440 1000 14400 1000 1400	王高高王	AME: 8480 18160 MMR: 10600 23400 1914 6000 13400	1400   15600   2600   18209   1200   25000   1200   25000   1480   19800   11200   25000	## 8 000   1000 22660 21400(1)  ## 10400 21400 2 8000 3400 4000 8)  ## 1000 22400 3400 4000 80  ## 1000 22400 32000 3400 10  ### 1000 22400 32000 3400 10  ### 1200 22400 3200 10  ### 1200 22400 3200 3400 10  ### 1200 22000 2200 3200 10  ### 1200 3200 3400 3400  ### 1200 3200 3400 3400	9000   18400   5.000  anno 13500   40000    10600   21800   29604 3600   42000   0)   11600   2.9604 3600   13500   0)   10600   2.9600   23600   0)   10000   2.000   28.000   34.00   0)   10000   2.000   28.000   34.00   0)   11600   2.6400   3.500   0)   11600   2.6400   3.500   0)   11600   2.6400   3.500   0)   10600   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.6400   3.500   0)   10000   2.	MALL 9000 1840: \$3000 3.0000 3.0000 1860
	ŀ	Now Lusercates (Lusercates) (Lu	M Now Lussocates Toeques Few Hens Toeques From Nut Toeques Few Heas Toeques From Nut  Manuel Strees (*Nut)  Manuel Strees (*Nut)  Manuel Strees (*Nut)  Manuel Strees (*Nut)	TORRULD FROM HEAD  TORRULD FROM MAT  TORRULD FROM MAT  TORRULD STREES (**In.*)  TORRULD STREES (	Tokewer Fram Heno   Tokewer Fram Mit   Tokewer Fr	TORQUEO FROM HEAD   TORQUEO FROM NUT   TORQUEO FROM NUT   TORQUEO FROM FROM   TORQUEO FROM HEAD   TORQUE	TORQUEO FROM HEAD   TORQUEO FROM NOT   TORQUEO FROM NOT   TORQUEO FROM HEAD   TORQUE	Tracture from the policy   Tracture from the p	Trecuest Free   Free	The control from the first   The control fr	

---- N, 1/2 -12 UNF-3A

NUT ---- E8 - 242

TORSION - GA SCREN OR BOLT - MS-20024-52 MAD BY AIR RAFT BOLT CORP. EL MONTE, CAL.

MED. BY ELASTIC STOP NUT COKP, UNION, N. J.

TEST DATA CONTRACT Nº AF 33 (616) 2808 P-1227



SCOTCH SHOWING HEAD COUNTERSINK IN HARDENED STORE SHOWING BLOCK (ROCKWELL (C. SCHIE 60)

WAD	Non Lusa	RICATED	LUBRI	CATEO
8 ~	Toequed Feom Head	TORQUED FROM NUT	TOROUGO FROM HEAD	TORQUED FROM NUT.
70 \$	TENSILE STRESS ("/w")	TENSILE STRESS (4/N2)	J TENSILE STRESS (*/IN*)	J TENSILE STRESS (*/WZ)
57	10,000 30,000 50,000 70,000 90,000 110,000 140	10,000 30,000 50,000 70,000 90,000 110,000 MEO PANTE 1 1000 (1)	10,200 30,000 50,000 70,00 90,000 110,000 110,000 110,000 (a)	10,000 30,000 50,000 70,000 90,000 110,000 WEED PRINT
330	(bi-") (b	M 6000, 1:870 Z86U3 36400 43000 49400	10 1 mare place torque torque torque torque torque (10-1) (10-1) (10-1) (10-1) (10-1) (10-1) (10-1) (10-1) (10-1)	M-1 2000 5200 8400 11600 560 2000
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N 4H CH AVE.	10450 21000 28020 35020 41002(1)	# 9000 21400 40407 51000 44000 51200 # 8600 18000 26000 31000 44000 51200	4Ht 2400, 5200 7800 11000 1400 19802 5Ht 2+00 5400 8400 11600 15000 19800	41/4 - 2000 4600 7600 1040 1/3400 18000 51/4 - 1800 5800 9000 12400 16000 21000
X MAX	15000 27000 37000 44600 53000	145 9240 19760 2980 86120 42440 48840	Miss 2200: 5000 7600 10720 14420 1884/1 Max 2400: 5400 8400 11600 15000 19800 May 1800: 4400 6000 4400 18000 17000	1200 5400 8600 12120 15880 20880 1000 12120 15880 10880 1000 1000 1000 1000 1000 1
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NW. (5007 HEAD) VERSEY	Now LUBRICATED	TOROURO FROM	TENSILE STRESS	as sa as as as as as as as as as as as a	A DEANE DESUE DEANE DESUE DESUE DESUE RESUE	367 / 1/40 82 132 198 290	0 84 130 188 274	(1) / 40 80 125 176 228	(1) Apr. 18 83 128 175 254 33	1000. 16 84 132 198 290	400 1 10 96 011 001 001	(1) 2W 46 146 234 307 374	3N 96 250 355 453 535	60 132 198 275 345	75 189 276 359 441	Max. 96 250 355 453 535 Max. 46 132 198 375 325	110 240 352 437 506	W 75 195 288 382 456	110 265 390 500 578	87 233 331 458 549 6-	91 222 329 429 506 56	71 175 285 370 443	117 261 379 479 542	34 10 245 376 480 552	93 237 334 447 524	90 245 358 473 557 62	117 278 397	07 070 053 447 524	106 045 385 465 508 545	Survered 3V-105 268 382 471 548 597	712 (1500 250 362 478 567	72 485 584	8 712 MARK 106 275 385 485 584 646	362 445 508 5	DEGUNG OF STREW SPECIMENS. OF THE RUN TO INDICATE WITH
TEST CELL — N.C. TRESSON — TB A MP. BY ARRO POTT SCHEM G., STANTOBO, CANN. (SUT HEAD) W.D. BY ARRO FORD AUT CARE, UNION., NEW JERSSY	Nov Lubercated	TOROURO FROM	TENSILE STRESS	as sa as as as as as as as as as as as a	A DEANE DESUE DEANE DESUE DESUE DESUE RESUE	295 367 / 1/40 82 132 198 290	255 (7) 22 30 68 111 157 222 2553 0 30 189 274	392 (1) 40 40 80 125 176 228	344 (1) AN 36 83 128 175 254 33	4.25 198 290 250 198 290 259 250	445 400 \ W 96 01 001 001 001 445	461 (0) 20 46 146 234 307 374	329 m × 34 96 250 355 453 535	(1) (W) 60 132 198 275 345	411 Ave. 75 189 276 359 491	329 Man 46 250 355 453 535	503 505 / 110 240 352 437 506	2W 75 195 288 382 456	(1)	(i) 54 87 233 331 458 546 6	100 922 329 429 506 56	71 175 285 370 443	RUPTURED / 1/1 261 379 479 542	0)	(1) / 40, 93, 237, 334, 447, 524	(1) / 30 245 358 473 557 62	Mar. 117 278 397	07 070 053 447 524	106 045 385 465 508 545	507 (Suprage Suprage) 30 105 268 382 471 548 597	688 712 Wasser 44 100 250 362 478 567	72 485 584	619 688 712 MARK 100 241 373 472 584 608 123	362 445 508 5	DEGUNG OF STREW SPECIMENS. OF THE RUN TO INDICATE WITH
TEST CELL — N.S. TEST CELL — N.S. TEST CON — TB  CONDESSION—EB  D BY ARRO PUT'S SCHEM G., STANTOBO, COMM. (SUIT HEAD)  2. PY EMNTL, STOP NUT CARE, UNION, NEW JERNSY	Now LUBRICATED	FROM	STRESS ("ILM) J TENSILE STRESS	as sa as as as as as as as as as as as a	A DEANE DESUE DEANE DESUE DESUE DESUE RESUE	149 227 295 367	144 196 253 0 X 30 46 84 130 188 274	217 315 392 (1) 40 40 80 125 176 228	(4) 21/ 344 (1) Aut 36 83 128 175 254 33	144 145 259 1100 110 84 132 198 290	304 300 445 400 \ 11 06 01 021 021 021 021	31039946100 / 20 46 146 234 307 374	222 279 329 m X 34 96 250 355 453 535	395 485 0) ( 20 132 198 275 345	323 404 411 Ame 75 189 276 359 491	222 229 329 May 461 132 198 535 345	360 448 503 505 / 1/0 240 352 437 506	386 454 - 20 382 456	475 540 60 500 578	438 510 (1) / SU 87 233 331 458 549 61	386 458 429 506 56	275 328 Man. 71 175 285 370 443	305 SLOT RUPTURED / W 117 261 379 479 542	331 404 0)	490 592 (1) \ 40, 93, 237, 334, 447, 524	457522 (1) 30 90 245 358 473 557 62	592 MAN. 1.17 278 3.97	707 704 447 524	247 108 075 385 485 508 345 247 108 075 385 483 581 634	373 456 507 (Figure 12) Marrier 30 105 268 382 471 548 597	505 610 688 712 000 40 100 250 362 478 567	72 485 584	500 610 688 712 MAN 100 275 385 485 584 646	362 445 508 5	DEGUNG OF STREW SPECIMENS. OF THE RUN TO INDICATE WITH
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TOST CELL — N.Y. TOST CELL ELECTRONIA CELL STANDED CONV. (SLIT HED) — AN 365-534 — N.D. P. ENSTR. STOP NUT CAR. UNION., NEW JERSEY	Non Lubricated	Toequeo Ferm Head Toequeo Ferm	TENSILE STRESS ("I'AL")	प्रकार आक्र के का महत्त्व के का महत्त्व कि का महत्त्व के का का महत्त्व के का का का का का का का का का का का का	of Version with the property of the property of Version and the property of th	7 33 91 149 227 295 367 W 40 82 132 198 290	34 91 144 196253 0 X 30 46 84 130 188 274	4W 106 134 217 315 392 0 / 4W 40 80 125 176 228	AIR. 5% 1/3 /9/ 221 344 AIR. 38 38 128 175 254 33	MAR. 166 165 249 340 425 MAR. 46 84 132 198 290	14 99 230 304 390 445 400 \ 11 0 96 211 221 221 125	24 102 222 310 399 461 (1) 24 46 146 234 307 374	70 163 222 279 329 m X 30 96 250 355 453 535	34 131 290 395 485 0) 4W 60 132 198 275 345	AIRE 105 238 323 404 411 Ave. 75 189 276 359 411	MILE 120 163 222 219 329 MILE 11, 132 198 325 453 535	110 260 360 448 503 505 / W 110 240 352 437 506	24 106 261 386 454 200 MILLON 2W 75, 195 288 382 456	# 34 600 6 15 338 (1)	54 145 315 438 510 (1) \ 54 87 233 331 458 549 61	386 458 470 540 36 406 41 222 329 429 506 56	94 200 275 338 May 71 175 285 370 443	74 96 310 300 5107 RUPTURED 1/1 1/7 261 379 479 542	34 105 288 331 404 0 3 4 10 2 25 376 480 552	150 352 490 592 (1) / 40, 93 237 334 447 524	34 147 342 457552 (c) 30 30 245 358 473 557 62	Max. 156 352 490 592 Max. 117 278 397	TEST DISCONTINUED TOTAL 10 07 237 334 447 534	24	34 107 257 373 456 507 (September) 34 105 268 382 471 548 597	150 370 505 610 688 712 (100 250 362 4 78 567	24   43   335 478 572   635 680 me 2 90 240   372   485   584	150	(1) Due To THE Screen During 600 1 4701. 90 340 362 445 508 5	DEGUNG OF STREW SPECIMENS. OF THE RUN TO INDICATE WITH

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2. STANTORD, COUN. (PHILLIF HEND)	TORQUED FROM NUT	TENSILE STRESS (#/1,12)	A seave many many many many many many many many	387 502 585	108 310 525 704 848	80 215	108 210 345 483	127 325 580	520 662 802	185 497 750 944 1100	54 175 405 635 830 1005 (1)	164 397 617 802	127 325	210 510 740 900 1082	2N 140 435 640 825 982 (1)	185 470 720 950	190 525 760	535 8/2 1025	255 533 767	160 473 684 880 1098	45 170 450 675 850 1008 (1)	BOLT YIELDED AT END OF 3 ED TO	ANA. 225 533 795 1045 1205	100 450	550 785 950 /087 (08.00.00.00.00.00.00.00.00.00.00.00.00.0	165 500 740 905 115 3000	200 500 770 1040	TEST DISCONTINUED AT 3 PD TORQUING	188 504 746 944 1116 (Shing rat)	0501 618 069	2 o €
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TEST CELL - Nºº ESEGON - 744718 COMPRESSION - 58. HED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND) MED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND)	NON LUBRICATED	TORQUEO FROM	JENSILE STRES	South of the south state of the south state of the southo	175 425	20 215 540 905 1090 1	20x 470 7/5 11/5 1	125 332 1590 8-10 1	115 540 905 1115 13	175 332 590 840	330 815 1045 1270	275 675 1000 1250	225 700 960 1210 1515	240 530 030 1213	340 75 74	1375 790 1125 1395	/ 2W 375 820' 1125 1440	3 75 755 1170 1305	3 5 745 1265 135	34% 760 1145 1375 1	300 640 1040	325 770 1140 1445	355 765 1090	375 775 1030 1270 1	375 885 1224 1565 12	346 782 1110 1396	300 715	325 790 1145 1485 1750	2V 320 755 1100 1350 1545	340 735 1035 1300 1535 (**)	etuesa	A 450 8 5 1140	306 735 1035	7 2 V
TEST CELL - Nºº ESEGON - 744718 COMPRESSION - 58. HED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND) MED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND)	Now LUSRICATED	TORQUEO FROM	JENSILE STRES	South of the south state of the south state of the southo	840 (2000 Hills) (175 425 6	- MEAU RUMUNED \ 20 215 540 905 1090	W 205 493 759,100	3/ 1/25 332 1500 8-10 1	115 540 905 1115 13	10 KHO KHO	24 330 815 1045 1270	34 275 675 1000 1250	40 225 700 960 12.0 15.15	Aue. 247 (34 92) 12.39	340 75 74	1375 790 1125 1395	2W 375 820 1125 1440	80PTURED 30 1305	3 5 745 1265 135	34% 760 1145 1375 1	300 640 1040	325 770 1140 1445	355 765 1090	375 775 1030 1270 1	375 885 1224 1565 12	346 782 1110 1396	300 715	325 790 1145 1485 1750	2V 320 755 1100 1350 1545	340 735 1035 1300 1535 (**)	4W 300 700 1125 13901665	An 450 8 5 1140	306 735 1035	7 2 V
TEST CELL - Nºº ESEGON - 744718 COMPRESSION - 58. HED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND) MED. SY REEG BOA'S SEERI CO. STANDARD GAIN. (FRONCOM HEND)	NON LUBRICATED	FROM	JENSILE STRES	South of the south state of the south	840 (2000 Hills) (175 425 6	- MEAU RUMUNED \ 20 215 540 905 1090	W 205 493 759,100	3/ 1/25 332 1500 8-10 1	1700 215 540 455 1115 13	10 KHO KHO	24 330 815 1045 1270	34 275 675 1000 1250	40 225 700 960 12.0 15.15	100 340 530 830 12 5 10 12 13 10 12 13 10 12 13 10 12 13 10 10 12 13 10 10 10 10 10 10 10 10 10 10 10 10 10	13 1045 13	/ // 375 790 1125 1395	2W 375 820 1125 1440	80PTURED 30 1305	3 5 745 1265 135	34% 760 1145 1375 1	300 640 1040	325 770 1140 1445	24/ 355 765 1790	30 3.75 7.75 1.030 1.2.70 1	50 375 885 1225 1565 10	346 782 1110 1396	300 715	325 790 1145 1485 1750	2V 320 755 1100 1350 1545 "	340 735 1035 1300 1535 (18	30200000 1125 1370 1665	375 July 75 1140	306 735 1035	18.80 V 0 V
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TEST CELL - NE TO DANIGGY ST FERENCE - THATAS TO MESSAGE SE COMPESSAGE SE TO NA SOUTH SA MED. BY REE BOY & SERVICE, SHOOL (FRONCOM HEND) MED. BY REE BOY & SERVICE, SHOOL (FRONCOM HEND)	Now LUBRICATED	Toequeo Fean Heno Toequeo Fean	TENSILE STRESS ("IM)	See a cocie accie accie accie ( )	14 145 350 640 840 1800 1800 1800 1800 1800 1800 180	3.9.3 (44.02) - HEAD RUPUNED \ 20 215 540 905 1090 1	44 1801550 W	24 225 885 10 10 10 10 10 10 10 10 10 10 10 10 10	MARX 225 5-85 (10 90)	350 840	20 330 815 1045 1270	34 255 570 (A) 34 275 675 1000 1250	44 1315 665 0)	Aprel 3.03 (10) 12 (24) 5.30 (	Max 340 22 20 1045 13	// // 375 790 1125 1395	2N 375 820 1125 1440	24 376 (1) 7555 HILLIN RUPTURED 34 375 755 1170 1305	54 4 0 0 0 12 12 12 12 12 13 15 14 5 12 65 13 15 13 13 13 13 13 13 13 13 13 13 13 13 13	ANS 347 760 1145 1375 1	Max 305 640 1040	W 325 770 1140 1445	24 355 765 1090	300 (1)	54 425 (1)	1396 1110 1396 1	Min 250 Min 200 715	M 325 790 1145 1485 1750	24 320 755 1100 1350 1545 "	34 300 days to proper the properties 34 340 735 1035 1300 1535 1035	44 323 Tright Sand State Contraction 44 320 Tright 13701665	430 000 875 42 77 30 1140	Max 430 875 1145 1	(1) TO PARAGA THE MATERIAL HEAD BY THE TOOL WHILE BLANKE FLOW THE PARAMETER TOOL TOWN THE PRESENCE TO SHEAT HEAD THE PRESENCE TO SHEAT TOOL TOWN THE PARAMETER TO SHEAT THE PROPERTY OF THE TOOL

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DRAMED FROM HERD

METO BY ELASTICSTOP MUT CORP., UMION, NEW JERSEY 89 -NOISSECHO

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(1) DUE TO STOT DENER TOOL (HARDINGS): ROTELLELLG-46) REGINNE DENEMING THE HOLD IN THE HAID IN THE SHEACHES TRUCKING VALUES THAT THOSE SHEAVEN (3) ELLOS OF LOCATIONES HEAVER MAD SHEAGHTHEN THE HEAD SHEAVEN OF HEAT SHEAVEN (4) ELLOS OF HAT OR HEAD SHEAVEN OF HEAT SHEAVEN

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SCREW OR BOLT - AN 509 - BIGE 49 METO BY AERO BOLT & SCREW CO. STAMFORD, COMM. (SLOT HEAD) N. 12-200NF-3A TRELYBAUNAL IS MOISSOL .5N - 7737139

DENDITA SCRETCE STIENS STONE LZZId ENGAIRES IN PRIRENTHESIS CONTRACT Nº AF 39(6N6) 2808 ATAU TES!

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Stercy Sybuma Haro.  Stercy Standard Black  Stan Standard Black  (Rockhall (* Scale 60)	LUBRICATED	TOROUGE FROM NUT	1	Agas Gaco logo marine Blace	1 1 ( ( ( ) 0 ) 39 0 7 0 0 1 1 2 0 ( ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	415 770 1140	ALL 250 200 1170	765	185 1155	MIN. SCHAFFE DATA SAFEET	DISCOUTING	150 4 70 B 2E	200 760	4 185 670 1190	Max. 188 532 898 1368 SEE ABOVE NOTE		0 1000	344 870 870 4880	1	175 750 (415 VIELDED			2000 000 1000 1500	275 455 845		AVE 324 630 0002		1/1/	244 1 35 420 800 1375 4300 Bort Melber	135 475 890 1350		2000	
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- No 7.8 - 7.8 Standeder Gain. (a.et nad). Union. New Jersey	САТЕ	TORQUED FROM NAT	J TENSILE STRESS ("MINS)	A more from more more mark than the more more	355 1375 2260	30 425 1345 2175	4		425	WW. 355 1345 2175	705		dw .	A18 1950	100x. 935 2100 2945		775/2/2/3			558 2200 3175		11/20 2580 34	2230	3V	70			1000 2365 3300 4025 43604 30LT.	790 2205 3300 4075	30	477	Add 940 2285 3300 4050	4075
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Alors: \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	CALEDICALE	Toesues from Heas	ILE STREES ("IMS)	अवक अनु का श्रिक का मान्या है। जिस्से का मान्या है। जिस्से का मान्या है। जिस्से का मान्या है। जिस्से मान्या है। जिससे मा	2	200 725 330 7210 MAC(p) 30 260 420 600 800 960	(1) 344. 80 210 360 520 685	440 700	500 725 590 1210 Apre 90 236	100 100 360 620 685	470 700 960 1180 11744 80 200 360 560 760	(1) 304 to 10	1 80 000 080 350 380 000 000 17/7 I	3421,000 240 440 700 340	470 700 960 1180 Aut. 88	015 026 000 80 run	3.50 770 1033 1300	08/	80 220 400 640 900	520 770 1055 1300 And 74 204 384 584	460 680 940	555 805 1090 1340	310 450 630 820	1) 3x 30 310 450 630 620	200, 540, 540	555 805 1030 1340 Ane 108, 271 456	May. 80 200 360 580 600 140	505 745 1020 1210 ((19000PH) 144 190 180 360 560 800 40	205 360 550 745	" " " 0) 30/2 L60 205 360 550 745 900		505 745 1020 1210 (MISSEN) TAKE 82 226 408 624 846	0401 040 065 080 000	720 (787)
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DATE - 34EET 2 OF 1 SHEETS (SEE 14.50 TEST DATA 24 414,1957) 57.22 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	NON LUBRICATED	Toequeo Festi HEAO	TENSUE STRESS ("Jax)	Secretary and supplied to the supplied of the	14 4 4 5 6 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	24 Ses 890 a	W 44 350 975 (2)	54 3.85 950 (a)	440K. 565	14 500 112.5 1600	5 55 (150 (2)	34 400 (225 (2)	443	AME: 480 1215 1600	Max. 555: 335	14 540 1375 1725 (B)	24 460 1375 (2)	W 500	5W 530 1425	M. 1913 (725)	Mus. 1460 1340	14 575 575 2000 RUNIO SECTED MEAD	34 600 400 (2)	4H 500 1510 (R)	3H 575 1545 (2)	MAX	500 1400	M TEST DISCONTINU	3 C C C C C C C C C C C C C C C C C C C	W 619 1635 2215 (2)	485 1575 2225 (2)	Mar. 610 1665 2360	West 485	COMBONELIES: (2) DUE TO SLOT, DRIVED TOLL (HARDAGES): POCKUGEL C-48) BREAKING LIMINE THE

Skéteu Shewmik héar Chamterskilk in Héarskild State Shakme Beag Rockhell (* Stale 60)			. NUT	STRESS ("/W.")	20,000 80,000 105,000 130,000	0 0	15 20 25	20	15 18 20 %	14 16 35	15 19 22	14 19 21	20	2	15 19 22	17	20 22 3	20	23	15 19 121	16 23 26	(3 (8 + 3/ 1 - 3/	0 c	23	+	16 2 64	7. 73	15 20 23 DB	15 120 25 BK	25 29	53	16 21 25 333	19 25 39 138	Processor.
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	acos.	Transe Come Vers	- 11	ILE STRESS ("/IN")	700 201 000,08 000,02 000,02 000,03 000,000,	16 20 23	16 20 2	15 20 21	16 2/ 3	15 20	/5	13 19 20	15 19 21	15 20	0,	+	15	6 / 4/	15	(2 /5 /9 32	25 25 23	F	6 1 91	0	14 16 20 22	15 19 2	15 19 20	15 19 23	17 20 25	+-	2000	69 63	1 15 18 22	REW) SAKEWS WERE NOT TORONED US OF MUT OR HEAD BENEAUS.
7657 DATA COURSES LA H 35(M) 2808 16	0	The state of	Same S	A TENSILE	10,000 30,000 10,000 30,000	114.2 4 8 214.2 4 8	0	542 4 8	50/	1 4	144 4 8 (2	4	4	SW-6 4 8 12	MAKK, 4 S	111111111111111111111111111111111111111	3 6	7.	200	20%	Max. 5 3	11 7 4 2-11	3.08	34.2 4 8	v 4	7	3 7 7	8	9	24. 4 00 C	4	Ave. 4	10101	THOW (SEE DATH SHEET ON 'D'SCI ON AND SUBSEQUENT WERKPING OF HEAD SPRICE BLOCK WAS SAND
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ж (эыт неяв) Л <mark>агээх</mark>		TOROUTO FROM MUT		ISILE SIRESS ("IIV")	20,000 10,000 50,000 REALE TREALE PREVIE (A. ") (A. ")	22 31 42 29 35	(V) (	23 32 43	52	3.9	24 32 43	35	9 C	4	25 35 45	4 33	28	480	n c	77	21 28 35	7 E	3 30	10 10 10 10 10 10 10 10 10 10 10 10 10 1	3 -	+	23 30	2 30	25 33 40	7 CO	4 30	ار ا	22 30 40	To A Boy 6 - 90,000 PSJ IN DR. NOT ON THE NUMBER TO INDICATE CONTOURS ONLY BUE TO SEARCH
ST. COLL - No.   DOWNERS   COLL - TB - COLL - TB   MID BY BEED BOLT E STEEM CO. STRANDERD (CONV. (SACTHERD) MID BY ELOSING STOPMET (DORE, WALDER)	LUBRICATED	704	7	730	1000 30,000 50,000 50	24 6 5			MAX. 8 16	7	20 6 14	g	1	$\mathbb{H}$	Marx. 1 16	11/16 15	. 7	200	10	1) 6 man	MM. 6 15		1	200	180	MAKE. 7 16	MIM. 6	Ø 6	3/2	000	φ	Mox. 1	MW. 6 15	CANANGE INTERPRETATIONS THE SOCIAL BY AND LEAD AND THE BECOMENT. CACH SPECIMEN FOR THE DEX
7650 Com SMAER BOLT & SCH BY ELASHC STOP M	NON LUBA	083	10/10	Transfund Comme	105,000 130,000 108.00 130,000 (HI-M) (HK-M)		3 3	1-1			1			П		(2)	_ [ ]	<   32   32   32   32   32   32   32   32	17					1	(3)			0	100 P	4 5	S	56	15. 60	OF HENDINGS VIOLENCY AND VIELDINGS ARE MARKED UNIVERSELVED UNIVERSELVED OF THE STANDOWNE OF
10 JANUARY 19 "W" 6-32MF. 3A		TOGOVED FROM HEAD	TENSILE STOFEE (#/1.2)		120.000 50.000 70.000 80.0 120 16 160 160 160 160 160 160 160 160 160	77	18 04 32	25	13 18 25 24	13 00 00 3 2	19 26	16 23 32 40	7 C	23 29	13 19 26 35	15 24 31 38	24 30		27 35	17 25 32 39	24	25 33	00 00 30 40	25 /35	18 27 36 40	20 29 39 47	25 31	10 20 30 45	200	16727 35	230 35 440 5	20 35 44	16 26 35 43	DUE IN GENERAL WAS AND THE TOWN OF THE THE THE THE THE THE THE THE TOWN OF THE THE THE THE THE THE THE THE THE THE
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es also been in my statement compilion (see Dath Spiet on 10 sector) sectors used por passaged aspec others in If the Bay to buildings unique to sectors and to seeked our underboints of factors for Ald Baylons, Superfects, Then bour but to wanted a Countaint of Medo Strict Sectors in Single, with enterfectors and product.

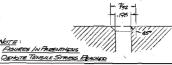
Setter Showing Has Courses Swand Brakes Tree Swand Bear (Courbeil C Some 60)	ITEO	TORQUED FROM NUT	TENSILE STRESS (#/WI)	कार्या करिया		31.16 3 8 16 26 34 45	90 /4 21 29	4 9	14 20 28	244 5 15 25 90 59	22 11	10 15	17 26 35	15 21 29	2002 6 15 25 41 48 52	25 35	2 10 17	5 1/ 19 29 37	32	246 4 9 19 22 29 35	05 /6 6/	14 3 8 10 20 31	4 . 9 /6 22 31	3 8 14 21	144 9 15 26 37 -45 75	10 20 23 30 41	404 3 10 16 24 22 65 75 86	4 12 17 23 27 31	May 6 12 20 28 42 44 65	3 9 15 23 27
COURTEST DATA  COURTED TO THE 35 (LW) 2909  NOTE: Forest Friest Region Services  COURTED TO THE SERVICES OF FRIENDS OF THE SERVICES OF THE SER	LUBRICATEO	TOROUED FROM HEAD		भी मार्याय मार्थाय मा	7 25 34 40	9 /9 26 72 38 // /6 20 24 26	1 2 4 3 45 50	32 45 50 M	1 20 24 26. M	(3 (9 26 30 33	6 // 20 27 x6 40	2 8 15 21 30 36	6 13 20 27 36 40	24 28	2 2 16 21 25 29	62 25 67	2 8 15 23 32 38	6 12 20 23 30 35	,	8 (4 /9 26 31	21 24 26	20 30 35 15 1 14 20 30 35 35 15 1	30 35 4	1 7 14 19 24 26	34 38 41	3 10 15 21 24 31 39	2 7 15 22 31 39 50	42 50	23 24 42 50	76 37
- No - 70 - 70 - 00, STAMFORD, COUN. (PHILLIPS HEND) CORP. UNION, N.U.	1	FROM NE	JENSIL	A GOOD STOOD STOOD PLOOD PLOOD HEST BOOK	20 8 02 26 36 50 65	9 16 31 45 63		4 2/ 33 45 63	5 15 26 40	29 47	0 0	49	Mari 2 21 32 44 62 75	6 /6 29 42 6/ 8	9 12 33.	40 8 19 34 49 65 94	23 35 48 59	0	6 /8 30 45	39 46 57		13 25 31 45 56	12 23 33	30 45 54 67	7 20 32 48 70 94	10 22 36 52	10 23 35 50 70 89	AN 14 25 39 50 60 67 78	76 74	THE THEORETICAL VIELD POINT AT END
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12 APRIL 1956 --- A-A 10-32 NF 3A COMPRESSION - 5A

MFD. BY AERO BOLT & SCREW CO., STAMFORD, CONN. " FLEXLOC DIV OF STANDARD PRESED STEEL CO. JENKINTOWN, PA.

TEST DATA CONTRACT Nº AF 33(616) 2808 P-1227



SKETCH SHOWING HEAD FILLET CLEARANCE IN HARDENED STEEL SPACING BLOCK (ROCKWELL C' SCALE GO)

WAD	_		Non Lus.	RICATE		`							<del>-1</del>	<u>Qaragr</u>	E LENSILL	U AZS		UBEI	CATEL		<u>-</u>	-	·		<del></del>	- 10
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됬	1 1/2	د.	TENSILE STRESS (*/wx)	١. ،		TENSIL	E STRES	5 (*//	(w2)				TE	NSILE	STRES	55 (*/ <sub>1</sub>	(NE)				TE	NSILE	STRES	55 (*/w	x)	
ų	SOM	el Me	15,000 32,000 45,000 60,000 75,000 90,000 Hest PT HE P	Zilya.			000 60,000	-	_	man	_C ∧:				60,000			HERRITICAL MELD PT. 11.000	Charles.	15,000	<del>_</del>	45,000	60,000	75,000	gan ?	111,000
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L. BOLT AN PIELDED AND DEVIKE MARK APPROMENTING OF "POINT OF FIRST TORGUING. IEST ON BOLT AN DISCONDINED.

1. BOLT SI SI SI AN AN ANT TERQUED TO GAT POINT (\$9,000 PS) AN EVID OF SELS TORGUING. PERSONNELL SIELDING PEIDE TO \$100 PS TORGUING, BY CONTINUED TO \$100 PS TORGUING.

3. BOLTS 31-1 AND SN-L YELDED. BEFORE ATTAINING THEODERICAL WELD VALUE OF HISODORY AT END OF \$100 PS TORGUING.

4. NICH MILES OF TORGUING FOR FIRST TORGUINGS OF BOLT AND SELECTED BY THEM BUSINES OF LORSE WALD VALUED TORGUINGS ARE ANALOD WITH AN "E AT THE DEGINNING OF THE RAN TO INDIREST MITTIRE, LYBRIGHTON AND, SUBSEQUENT LYBRIGHTONS OF NUT OR HEAD DEARING SURFACES.

5. EXIST OF LORSE WALD TORGUINGS ARE ANALOD WITH AN "E AT THE DEGINNING OF THE RAN TO INDIREST MITTIRE, LYBRIGHTON AND, SUBSEQUENT LYBRIGHTONS OF NUT OR HEAD DEARING SURFACES.

G. THE SPACER BLOCKS WERE SAMUEL AT THE UT 6TH TORQUING FOR THE DRY CONDITIONS ONLY DUE TO SCARRING.

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TEST CELL - Nº SERION - 78  SERION - 78  COMPRESSION-5A  RERO SUPPLY MFG. CO., IMC., CORRY, PA  ELNSTIC. STOO NUT CORP., UNION, N.J.	Now LUBRICATED	 		See is 1	37.76	AVE NAOX.	11/	36	35	Mex.	13/	2N	40	HVE	MIN.	3 3	34	50	MAK.	11/2	3 8	4K	35	Mex	The state of the s
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\&   \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \		so Fee	STRE	60,000 75,000 TORENE TORENA (M*)	130	135	258	235	300	300	300	276	329	307	727	2/5	352	328.	737	333	205	127	355	377	TED TORG
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Barr - A	-	`	Ē	30,000 1018241E (141.2)	78 63	14.		205	199	149	150	137	174	154	/37	/59 /4B	121	791	1487	797	174	/92	1,60	192	1 Runs
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या साम्या है।	. V	)	aN 5	present	prinosog	ואועואר	54	rina	94 ŏ	77		המנונית	ricy	#F	$\int$	5VI	nsac	2 102	p	9)	VI/X	200	Z FEE	5	] 3

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SHOWING HERE REPORTS IN HERE SHOWN BLOOK FILL TSCOLE GA			1/1007	57.8ESS 60,000 75 75.000 75	732	154	123	777	127	11/4	124	177	1	135			36	113	100	77	123	120	129	105	119		105
Skettu Shohiwa Hato Rizel Spolina Black Stetu Spolina Black (Eerkhetu Tii Siale 60)			1	PASILE NO 45.000	50/	26	ू इंट्रें	7/2	78	109	200	600	7.4	8 6	20 00	1000	77	83	2/6	2%	482	72 5	93	72	9 5	250	77
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2 e e	LUBRICATED	F		11,000 7000 PT.				Ť	$\stackrel{\square}{>}$		1			<u> </u>				$\stackrel{ extstyle +}{>}$	<u> </u>	7		200	362	326	2 24	1	
		·	1	000 06	296	362	394	296	276	263	364	364	220	275	205	263	2/2	26.9	222	306	327	205	┼╾╅	-+	202	++	244
COTE : CO			(a,/a)	2 2	230	243	332	2/2/83		2.70	305	365		22.9.	222	251		+.+	219	250	25.7	27.2	╁		279	₩	193
8 14 1708 Tensus		Torourso From Heap	STOREGE	60,000 TOROUE	180	207		120	1.1	+	-	150		18.2	207		H	++	154	H	100	2/2			77	╀	14.5
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808	}	Seque,	7	30,000 70000E 70000E	96		<b>†</b> ††	200	95	62	122	92	95	28	1/9	1611	38	16	100	27	307	30	201	20 1	1		76
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own, PA		NUT	(#/WZ)	75.000 CMANE	346		340	370	390	317	376	27.7	415	980	383	426	27.5	970	428	430	533	470	}	530	+-	536	455
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أ أو ا		NEO FR		01305	207	152	202	223	27/	196	100 m	76	265	299	2,90	307	_	<del> </del>	289	310	230	╂┤		3/3	╁╼╂	323	3001
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MED BY ARRO BOLT & STANDARD COIN.  "" " FLEXOR DOLT & STANDARD STREET COIN.  "" " FLEXOR DIV. OF STANDARD PRESS STREET CO.	NON LUBRICATED	-		TOROLE (M.*)					<u> </u>					$\times$				>		11		103,600 PS)	970	57.07	7507	1075	4.10 II
AERO L FLEXLOC	Non	0	(sv	90,000 TOKULE (W2)	988	765	200	740	800	200	27.79	740	763	825	795	292	767	275.2	825	8.28	25.3	~	040	84.1	873	995	7804 50
- [		M HER	STRESS ("/W.	75.000 TOKENE (1111:1)	445 820 640	545	820	564	665	272	212	795		733	645	233	# ─	205	-	230	7.45	826	730	750	720	826	" DN'Ad'T
	<b> </b>	eo fee	STRE	60,000 10454E	525 639 522	430	325	425	555	588			55.5	578	547	6113	040	5.80	625	299	27,5	999	630		2.87	9000	BEGAN :
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Dare Size Exert of Bar- Wr				15.000 Men. ")	111	1/8	/27	174	L -L-	175	17.7	120	1-1	182	[	182	765	180	182	1 +	127	172	200	11	185	300	
DATE 51ZE (WT	Ç		7	- 1-38E-1	H. H. S.	37	MARK.	¥ %	THE !	F. 4.5	AVE.	14/	7.7	4	F.F.	MAX.	H	表	SH SH	AVE.	IMM	¥ 1	1.	1-1	13 4	Mark	

15,000 33,000 45,000 105,000 30,000 111,000 111,000 SLETH SHOWNG HERD FILLET (LEPRINKE IN HARDENED STEEL SPACING BLOCK (BOCKHELL (\*\*\* RAGE 60) TENSILE STRESS ("/W.) 185 172 220 TORQUED FROM NUT 140 dut 35 LUBRICATED 1500 3000 45,000 45,000 75,000 95,000 1110,000 1 NOTE:
HOURS IN PRESUMES COURSE
DEVOTE TEASLE STREES RECIED 55 125 205 285 350 425 355 168 225 277 TENSILE STRESS ("/IN.") 125 185 285 Toequeo Feom Head 100 150 3 122 182 5 205 285 1.25 027 225 140 /32 700 5 TEST DATA CONTRACT Nº Nº 33 (WW) 2808 120 24.2 L 20 34.2 L 40 44.4 L 25 2 44.1 7-114 P-1227 TENSILE STRESS ("//u2) TORQUEO FROM NUT TEST CELL - Nº.
TRESION - 1947B
COMPRESSON - 58 51 100 170 Ave. 105' 202 May. 135 260 May. 655 170 411 239 380 541 /15 202 APAC. 163 280 APAC. 830 380 APAC. 190 202 270 15,000 50 105 Ave. 136 Max. 175 Max. 105 85 165 710 Now LUBRICATED 32 35 28 33 3 75000 90,000 Mess 11,000 1765 TENSILE STRESS ("/W.) Токачер Геом Нено 935 30,000 45,000 60000 760 745 535 675 670 445 525 570 705 475 545 695 555 550 355 425 345 520 423 424 520 352 485 320 370 376 400 15,000 175. 488 780 200 80 240 285 /80 À £ 15 15 1 0-0

WERNER (AND SOCKET, WARRICH RRICKED) IN END OF ON TRAQUING WHILE ATTEMPTING TO MITAIN YIELD POINT OF BOLT S SHOWS TAKE
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STATE SUBSEQUENT WIDGINIOUS OF THE OF THE SUBSEQUENTS 1. BOLT. 2H OF HON-LUBEINTED BOLTS TARBUCD FROM HEID, RECEINED RUFTURED HEID BY SOCKET BOLT BH. "" S. NEW HEIM TOTT M. SOCKETS WICKE PHIREDS FOR BOLTS AH & SH A. KHAS OF LUBBEINTED TORORINGS HE HARED WITH AN "L" HT THE DECHMING OF EACH TORORING FOR I

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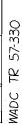
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TR 57-330 WADC

STATUS CHONNIG HEAD OF THE PROPERTY OF THE PRO	ARED	TORQUED FROM NUT	TENSILE STRESS (#/w.²)	0 20-	230 292 355	86 140 225 285 332	//2 200 262 327 355 //2 200 262 327 388	75         140         2.15         875           88         170         2.39         2.97	344 65 150 210 275 323 380	125 187 270 337	77 178 206 278 332	MAN 65 123 187 270 308 380	246 95 175 233 325 392 468	70 /35 200 270 340	1/2 185 240 325 357	╌┞╌┼╌	120 175 295 305	34 75 150 220 295 350 490	55 100 162 250 315	14. 124 126 260 213 524 400 188 264 324 400	55 100 162 245 305	95 150, 220 282, 325 395	344-65 135 235 300 365 425 520 444 70 135 305 305 305 305 600 500	4 98 175 245 295 365 490		740 (3) (3) (4) (5) (3) (4) (5) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	665.
Courgest 18 AF 39 (LAS) 2809 Wars: Ministeriors	LUBRICATED	Toequeo Fean Heno	TENSILE STRESS (*/n.º)	386	744, 56 248 325 412 525 244, 150 245 347 450 2515 600 344, 152 747 7047 000 6470 6470	1,155 335 418 520 520	234 343 438 517 643 535 418 520 590 740	L75 148 235 315 406 490		SAL-170 285 400 50B 575 655	2/9 3/2 394 478 571	75 (48 235 315 406 499	244 118 225 325 938 520 675	225 320 420 520	2 240 325 425 575 675 2 240 325 425 500 615	675	145 233 315 400	342 133 240 363 475 575 680	522 705	115 204 305 394 489 592	302, 000	220 340 430 990 630	444, 162 325 315 910 980 600 775 444, 162 325 995 550 675 895 1060	250 390 932 500. 610 810	1000 142 230 329 421 501 627 837 16 1000 1000 1000 1000 1000 1000 1000	TO ATTOROUMS, PERVENTING SWCESSIVE TOROUMS.  BEFORE KNOTURE OF THE HEAD BY THE SOCKET DRIVE WE	AND SUBSCOVENT LUBRICATIONS OF NUT OR HEAD BEADANG SURFACE
CO. STAMPORD. CONH.  ONED PRESS STEEL CO. JENEWITHIN, PA.	SRICATED	TORQUEO FROM NUT	TENSUE STRESS (#/wx)	(1) (1:200 30.000 45.000 60.000 75.000 90.000 110.000	10 100 205 333 389 485 582 10 220 385 468 585 725 850 30 110 210 325 402 477 570	150 308 430 548 655		1/2 225 337 432 528	1/2 210 320 400 470	205 382 540 675	254 297 4442 561 6K1	210 320 400 470	2N 205 398 525 690 820 925	30 115 225 330 402 475 575 40 200 399 575 725 875 000	100 317 477 612 714	MARK 255 398 585 745 875 1010 MARK 115 225 330 402 475 575	295 442 547 630	125 245 328 4/5	40 250 425 500 820 952 1075 50 252 463 625 800 930 1030	625 660 775	158 320	20 188 387 580 745 898 1000		SN 210 455 620 805 933 1032	MAK. 273 497 573 858 MM 127 250 345 420	ED FROM HEAD, RECEIVED RUPTURED HEAD BY SOCKET WRENCH AN TORK TORY TORY TO AN TORY TO AN TORY TORY TORY TORY TORY TORY TORY TORY	THE AND THE DESTRIBING OF EACH TOROUNG FOR MITTAL LUBERATION. TO ACHE FOR MILE DESTRIBING OF EACH TO STREEM GO.
Date 21 MARCH 1956  Size	E-E	TOROUR		1500 30,000 45,000 60,000 75,000   15	225 #45 752 1235 (645 368 805 1/80 1552 1880	54 250 525 885 54 200 400 645 400 645	* WORK 1 2 5 15 180 1859 1879 3.011 WOLK 200 400 645 160 1875	24 5345 702 /225 1380 1700 2090	475 848 1/50 1485 1790	SW 320	MARK 475 848	1 410 775 1175 1400 1700 0150	24 325 740 1100 1428 1690		.  -	MIN. 3.10 6.25 920	24 350 770 1150 1479 1765 2005	945 /295 /6/0 /955	5H 300	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	IH HEAD KUPTURED AT END OF 4TH TORQUING	2 34 460 710 1115 1430 1720 2025 2438	44 395 760 1185 1500 1850 2185	325 690 1000 1285	Mar. 460 760 1185 1500 1850 2.185	COMMENTS: " I'M BOLT OF NON-LUBRICATED BOLTS, TORQUEL 3, BAY BOLT TO NON-LUBRICATED BOLDS, ARE MARKED TORGUNGS ARE MARKED TORGUNGS ARE MARKED TORGUNGS ARE MARKED TORGUNGS.	4. THE STREET BLOCKS WERE SAVOST ATTER THE SAME

WADC TR 57-330



W1 30										STACH	30 -	110 D W	_45 OF	13 56M , 13 4 X3H	15±1 00 31 <u>1</u> 1 ±0	0111 20 21 HANDING	776/1 76 52029	CONTRACTION OF THE PARTY OF THE	9/ 200	38 SL79	14 10m	May	א ובשאבונו	243 J LV	N WON'S	CONCOCC	J 27.008 J 27.0090	TRESCRIPTO	77-NONE	SLMA	wwo_	,
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· · · ·	-019	505	016	025		511			551	565	08t	59E	0SZ	001	MIN		0/8/	5011	526	SIL	505	OLZ	MIN	i <del>l</del>	SLIE	0597	OSIZ	5601	506	050	men	
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· /	500	088	015	958		081		<del>                                     </del>	E16	58L	050	DDS	668	682			8521	2701	028	520	DED	DEZ	314		6662	1122		55/1	DDL	05.5	316	3
<b>\</b>	000	085	050	588		181	+	11\	028	078	010	019	SSD	0621			5/1/	096	051	095	285	51%	NS	N /	58ZE	0002	5841	5021	59L	ODE	HS	5
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CONTRACT Nº AF 33 (616) 2808

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STATE SPACING BLOCK,

227 — DAN BC-37 MFD. BY ARRO BOLT & SCREW CO., STAMFORD. CONN.
—— BAN 363 C 820 " " FLEX LOC DIV. OF STAMPARD PRESS STREE CO., JENKINTOWN, PA.

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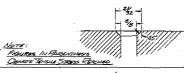
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MFD. BY AFRO BOLT & SCREW CO., STHMFORD, CONN. 

TEST DATA CONTRACT Nº AF 33 (616) 2808 P-1227



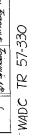
COUNTRESING IN HARDWARD STORE SPACING BLOCK (ROLLWELL C. 55,70.6.60)

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(2) ZINDS OF LIBERCATED TREAMED THE MAY "I" AT THE BEGINNING OF THE RUN TO INDITION INTIAL, WARRADOW & SUBSEQUENT LUBRICATIONS OF MAY OR HEAD BETWING SURFACE.

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STEE SPACING BLOCK
COUNTRESINK IN HARDRIND CONTRACT Nº AF 33 (616) 2808 SCREW OR BOLT - AN ILC- 62 MED BY ALRO BOLT & SCREW CO., STAMEDED, CONN. : <u>710N</u> 8180 IS31 BE. JNDII XX-2 5 AM 8 1 STELLY SHOWING HERO 82- WOVER

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TORSION -GAFGE

TEST DATA CONTRACT Nº AF 33 (616) 2808 FIGURES IN PARENTHESIS
DENOTETENANTE STORES PERCHED P-1227

SVETCH SHOWING HERD COUNTERSHIK IN HARDENED STEEL SANGING BLOCK (ROLKWELL (\*\* SENIE GO)

WAD		NON LUSE	CATED .	LUBRICATED
ĎC	4-6	TORQUED FROM HEAD	TORQUED FROM NUT	TORQUED FROM HEAD TORQUED FROM NUT.
Ħ	\$	TENSILE STRESS (*/w2)	TENSILE STRESS (*/N2)	TENSILE STRESS (#/WZ) TENSILE STRESS (#/WZ)
S	KIING	15,000 30,000 45,000 60,000 75,000 90,000 MED PARTY 11,000	15,000 30,000 45,000 60,000 75,000 90,000 HILD PAINT	15,000 30,000 45,000 60,000 75,000 90,000 110,000 115,000 30,000 15,000 60,000 75,000 90,000 110,000 1
1-33	12 3	TORQUE TORQUE TORQUE TORQUE TORQUE TORQUE TORQUE TORQUE TORQUE	13 5 MARINE TOWNE TOWNE TOWNE TOWNE TOWNE TOWNE TOWNE	The same record rooms were record rooms of the same rooms of the s
Ö	· > —	(H 3000 8600 /6000 24600 W)	W 4000 8 400 14200 23400(1)	244 1800 4000 7400 114433 1341
		2H 5400 12400 21800 31000 (I)	30 3600 8600 16000 25800(1)	344 2000 4000 6000 8000 10400 13600 444 2000 4000 6800 9600 13000 17000 444 2000 3400 5600 8000 9600 13000 17000
	1 1	SH 3,20/81 (5308 1800 (U)	50 4200 10000 17600 2 5000 (1)	844 2200 5000 8200 11200 150001 9000 9600 3400 5000 6800 9600 12400 1860 12500 12400 1860 1840 1860 6000 7960 12400 15520
	3 M	WK. 5400 11400 21600 31600 WM. 3000 1600 1600 24600	MM. 3200 7400 13000 2000	MAR. 2400 5000 8200 11200 15000 19500 MAR. 2400 4500 7200 9400 13 000 20400 MAR. 1800 4000 6000 8000 10400 13600 MAR. 1600 3400 5000 6800 8400 12400
	1 16	1H 7000 14200 (29.53 31205 (1)) 2H 3500 (400) 21000 30000 (1)	W 7100 13000 20000 26400 01	144 4000 6000 8400 11 200 16200 16200 144 1800 3600 5000 6200 3800 12000 12000 244 1800 3600 5000 6200 3000 11200 1
٠	3	3H 7200 15601/420033450(1)	3N 8000 15250232031250 (1)	344 2200 3800 5400 7000 8600 10200 12200 444 2200 3800 5400 8000 10000 12600 444 2200 3600 5200 7000 8400 11400
	100	5H & 507   +800 22600 3 22000 (0)	5V 17000 13400 21000128400W	344 2800 4800 6400 8600 10400 12600 3400 1800 3800 5200 6600 8200 10 200
_	NA	045	And 7100 13600 20800 28240 MAY 8000 15200 23200 31200 MAY 6000 12000 18600 26400	MARX 4000 6200 9000 11200 14000 16200 MARX 2200 3800 5400 8000 12000 12600 MARX 2600 4800 6400 8000 10200 12200 MARX 1800 3400 5000 6200 8000 10400
24	1.	14 7000 1 1 1 2 4600 32 600 (I)	W 7400 13400 20200 27800 W 2N 7400 14000 20600 27600 W	144 3400 5200 7000 8800 10 800 13400 14000 244 1600 3000 7000 8000 10800 244 1600 3000 5200 7400 8000 11000
	1 2 -	34 7633 16400 2453335633(II)	3N 18600 16000 23000 30000 (1)	3/4' 2400 5000 6800 8600 10600 13000 4/44' 3200 5600 6800 9800 11600 13600 4/44' 2200 3400 5800 7200 9000 12200
	12	## 8000,1600-2422033220010	SN 8000 13600 22400 29000 - 10 SHEAR	344 2600 4600 6400 7400 10000 12000 3400 4600 6200 7600 10000 3400 3400 5200 6680 8240 1080
	B 4	7320 16320 24280 32880 1000 17000 24600 35600 1000 1700 1800 33400	1945. 7560 13960 21320 28430 1994. 8600 16000 23000 3000 1994. 6400 12800 2200 27600	MM. 3400 5600 8000 9800 12000 14000 MM. 2200 3800 5800 7400 9000 12000 MM. 1400 3000 4600 6000 7600 10000
	5	IH 17823 1/62332 27402 34800W	W 6800 12 800 19400 2 6000 M 2N 10000 18000 26800 3200 M SHOKE	1/4 2800 5200 7200 9000 10400 12400 12600 3000 4600 6200 8000 10600 244 2800 3200 4600 6200 7800 10200 13600 244 1800 3200 4600 6200 7800 10200
	1	2H 7200 15 920 23600 33400(1)  2H 16-2 (6c 2665 3500 1) Streets (3)	3U 8000 15400 22200 28600 (1)	344 2400 4400 6400 8400 10000 12800 3400 4800 6000 8000 10000 444 2400 4800 7200 9000 11000 3400 444 1600 3200 4800 8200 8200 11000
	1/2	4H 245 16 276 276 1 10 the BR (0)	40 6000 12000 2000 28000 (1) 50 TEST DISCONTINUED	5441 2400 4200 6000 7600 9000 1/000 5441 1400 2600 4700 5800 77200 9200
	7 1	7920 16240 26240 35120 1994: 8600 16600 27600 36400 1996: 7200 13600 73600 33	AVE 7700 14500 22100 28650 AME 10000 18000 26800 32000 MAIN 6200 13000 19400 36000	MAR. 2800 5200 7200 9400 11000 13600 MAR. 1800 3200 4800 6600 8200 11000 MAR. 1800 3200 4200 5800 7200 9300 1000
		IN 5400 13400 26000 37001 (0)(3)	W 8000 4600 20800 29400 SHEAR WELL UMTERQUIA	244 2400 4800 7400 9100 11200 14200 20400 244 1400 2600 4200 5800 7400 10000 1600
	mnc	2H 7000 (1, 2, 25000 36000 (0)(5)	30 8000 14800 21000 29403 W STEPRE	344 2600 4600 6800 9800 1800 15000 20000 444 12400 4800 6800 1800 1800 18600 1
	100	4H T: 7 U1 0:1 (45,700) 00+T BROKE (NOT NOT SHEAD (NOT NOT NOT NOT NOT NOT NOT NOT NOT NOT	4N 6200 12400 19800 26000 SN 7EST 015CONTINUEN	SHIZ 2800 4800 6800 8600 10400 12200 16400 3HZ 1600 2800 4200 5800 7200 9400 15000
	10	ANT 1.00 1546 2616 36 500 MAX 8000 17000 27800 37000	AM 7400 13933 20573 28246 MIX. 8000 14800 21000 21000 MIX. 6200 12400 19800 2600	Ave. 2600 4720 6840 8900 10760 13400 18200 4000 4000 1600 2960 4600 6240 7340 10360 11400 4000 4000 4000 4000 4000 4000 4
		Man. 5406 13400 25600 36,000	DRAWET THE BOOK BURNET TO PREVENT FAILURE OF THE BOLT ROOT AREA IN	

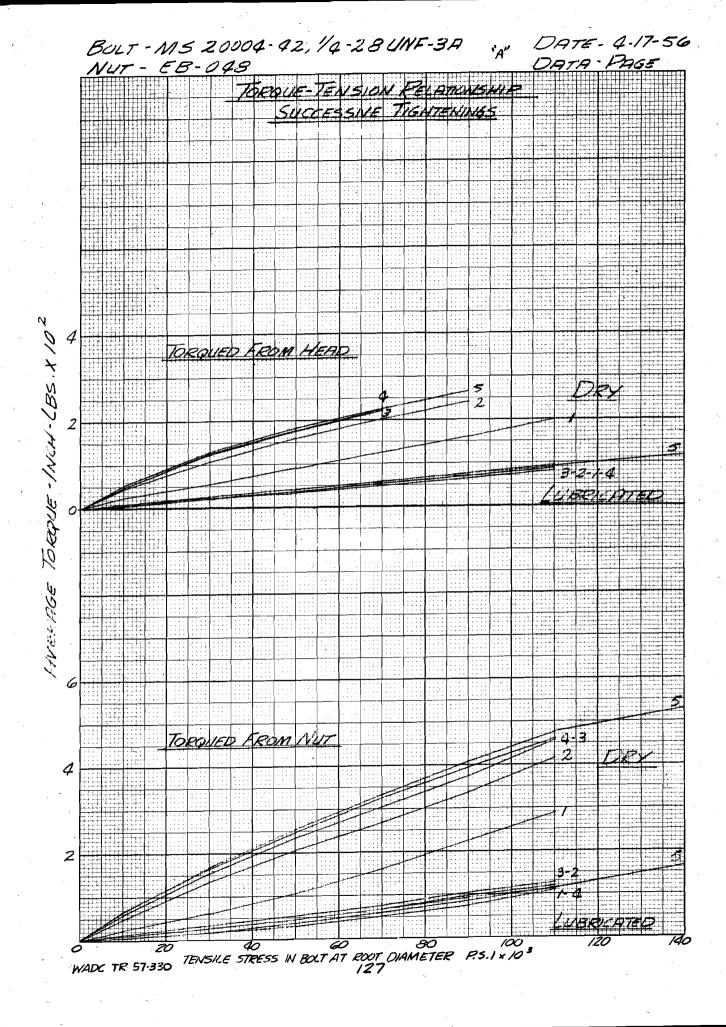
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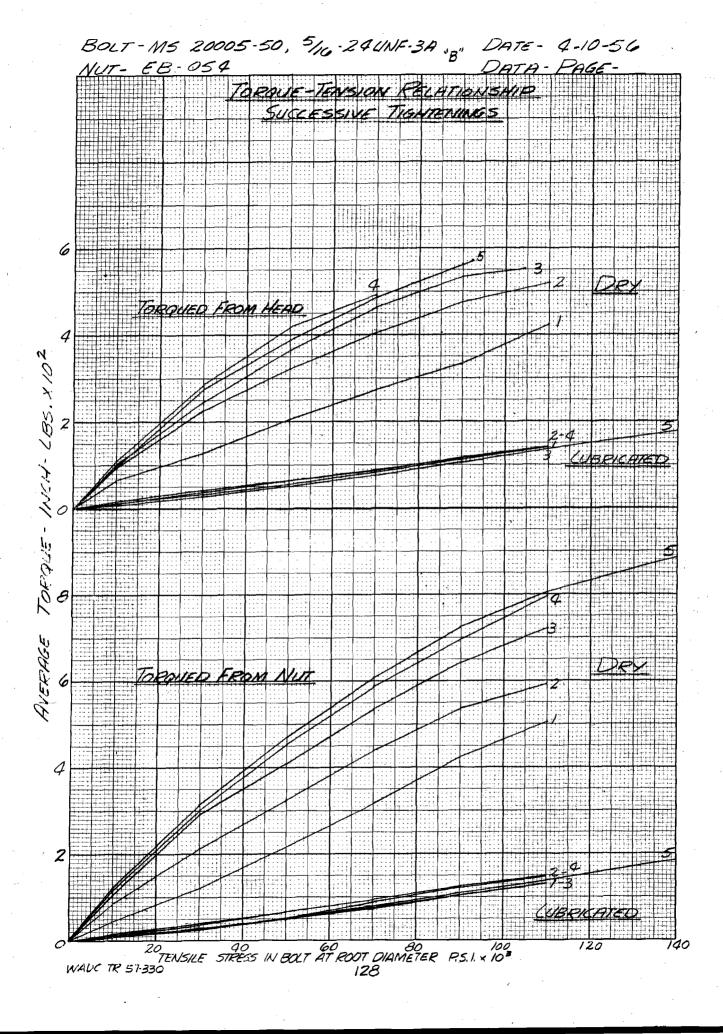
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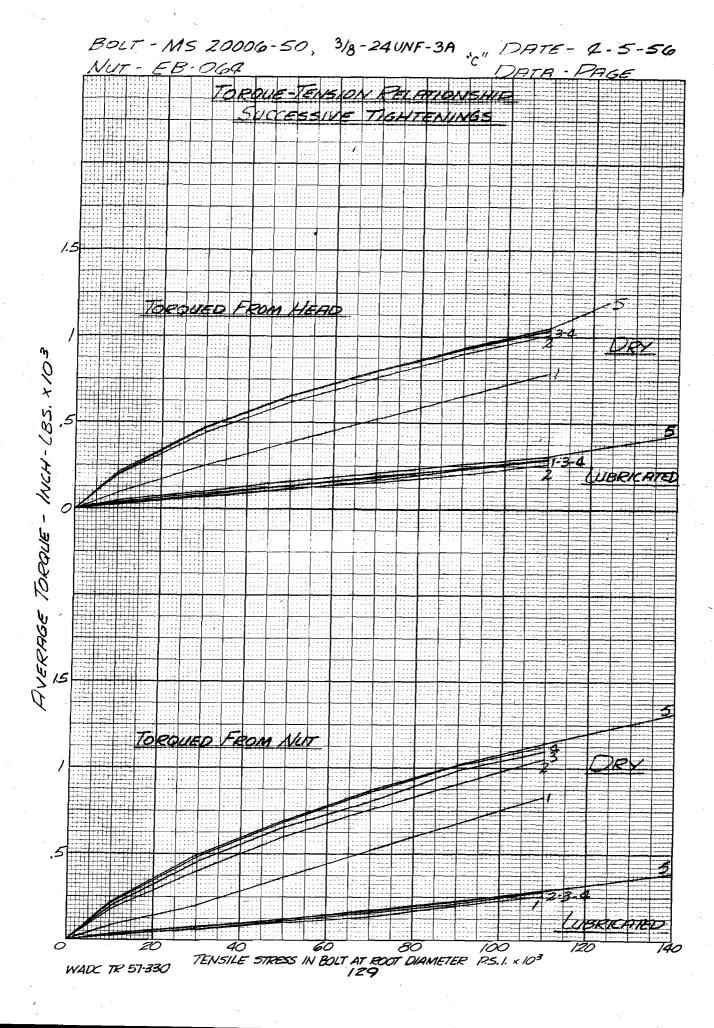
(1) Fine of tubelisted toke whate before the personance of the purity of the properties of the personance of the persona 17 20H 0.795H 00H16 00014 00H01 1940 00065 00988 000HF 00081 2024 08H05 008H6 06888 0H811 3A 000EZ 000 L 1 000 + 1 00 9 11 00 8 00 8 000 1 7.HP 0096 \$ 000 81 0000 1 00 9 L 0095 00 9 E 0091 7 744 Htz 24/2 000 2 600 1 0000 1 000 2 008 2 248 24-4200 6 400 9400 11 800 14200 1800 002 24 9000 17600 25800 33400 41000 W 14-5 2800 6000 8600 11200 13200 16000 2000 W 7000 15000 222032 36400 00 + 3E 600 2 5025 5 000 2 1 000 7 W 00861 008 24 00 46 00 27 00 42 00 88 00 41 7711 29 98 00001 0094, 0095 0096 0081 700 29 98 00001 0096 0000 0098 0098 0098 29 98 00001 0096 0000 0098 0098 29 98 100001 0091 0095 0098 0091 0098 778hh 07hLE 036/2 0776 MUI 078/5 07hEE 07hEE 077/1 XeW 7h7Ih 043/6 04h17 07/7/ AV 00051 00811 0096 0091 0005 0008 mull 0487 00441 00911 0006 0009 0005 www 04991 04861 04801 0988 4895 0818 24 00788 00018 00941 0001 NUN 00758 00098 00711 0006 NUN 07118 09688 09191 0808 2018 00291 00281 00901 0008 0095 000E , 7.HS (1) 00585 000 15 000 +1 00 57 Na (1) 0001 + 00+0F 0090 C 0096 HS mx - 1800 3 600 5 600 7600 10000 13 600 000710082100411004800820002144 AN 8200 16600 2440031400(1) (1) CO7+ + 00+17 00861 00707 HP (1) 000 1 E 00 + Z 5 000 T 1 000 E WE 344 2000 11 000 0000 1002 1005 12WE (1) COPE + OCO + COPES COOTI 3097 00011 0098 0099 00000 0097 776 00+8 N 00++ 0 0 9 11 0006 020 9 000E - 7-MZ ZILL-Z 600 4 600 7000 9000 12000 15600 (1) 008150037 40055 00501 00991 000 F1 000 11 008 8 008 5 009 7 7-H/ (1) 000 6 3 000 5 5 000 E 1 000 T W (1) 0082 + 0000E PO+07 0086 HI MA 2200 3800 6000 7800 104 00 13600 00868 00488 00051 0079 min 0000 1000 1000 10000 10000 0000 00588 20088 00008 20001 xew 02691 00081 09601 0758 0009 0808 my 00814 08501 08018 00001 My ante - 2400 5400 8400 11200 14200 16800 4N 8000 1 6000 2 4200 3 0 600 (1) (110001+00505 00005 00001) 44 00221 00221 00001 0008 0000 002E , 7.4E CU 000 25 600 33 800 44 0 00 (U) (1000826009260001 NE 000 21 000 21 00 28 00 07 0002 00 25 1 7/75 (1) 000 T + 000 E 5 000 E 00 5 01 HZ 2009 1 009 21 0086 002 C 008 + 00+2 ,7772 DOOB 1 008 +1 00311 0076 009 9 00+8, 7-17 M 9400 17 200 2 4 000 18 00+11000+100+110088 00+9 0098, 7.41 M-4 1 800 3 600 6000 8 200 10 808 1 4000 (1) 00 8 5 2 5 0 0 0 5 1 0 0 9 9 M (1) 0006 £ 0008 Z 0096 1 00 Z6 HI 00051 00A11 00AL 0075 0092 0031 MUU 009L1 00921 00701 00AL 0005 0092 XUN 0ASS 09171 0006 0AA9 022A 0217 XU 00116 00066 00421 0053 LUNN 0081H 0001E 30017 00HOI XOUN 0096E 04968 0000 \$ 0096 346 SULL 2 000 4 200 6 400 8 800 11 500 5 1 200 (1) 004 1 2 000 2 2 004 1 004 7 WG (1) 000 EE 0006 S 00 FE 1 00 FE NS 00051 000 1 000 8 00 5 00 1 1 00 1 5 00 0 dH-4 2 400 6 400 9200 12000 14600 18000 4H 9600 19600 28600 37000(1) 0098100+910008100+01009L000+7748 \$N 9400 18600 27600 37000 WE 110400 \$1000 30 60041 200 11 00 2 5 10 0 2 0 1 0 0 0 1 2 0 0 1 2 6 0 0 1 1 6 0 0 244 - 320d 66 60 9 90 01 2200 15200 1900 2N 8000 17 600 2 5 400 33000(1) (1)008 04 000 1F 000 1Z 00001 HZ 00051004H00+L00090008E008177/ (11000EE000ES 00+21 0083 W (1) 005 E 5 000 E 7 000 6 1 00 9 8 0009/ 00021 0006 0009 0004 0081 MIN 00961 00951 00911 0048 0095 0008 XXXXX 09661 00851 04001 0916 0454 0218 XXXX 0006,1 009H1 00901 009L 00HH, 00H1 MW 2029t 00461 00931 0005 NAW 0005E 0089T 00081 0076 NEW 0045E 084EE 08941 0469 344 00858 0084 t 10451 09187 08781 08761 09761 0006 0004 0000 09187 08781 08861 08861 0987 0878 309 00x14 00067 00881 0086 X600 E VS78 & DEFLI 09811 0911 3AV 00305 003 + 1 00511 008 T 003 + 0005 - 142 SUL 1 1800 + 000 0020 0000 12200 16600 SN 5600 15800 2460033600 (1) 00061 009+1009C1 007L 00++ 0091 , 7.HD 4H 1800 17400 27000 36400 (1) 00091 000 21 0006 0099 000+ 0081 7777 du 6 400 14400 2.5600 3.5600 11 DOFT 5 000 5 500 0 6 1 000 + 1 000 6 000 + 7-45 \$100 8 1 00 8 1 00 8 1 00 8 00 8 00 8 1 7/18 (1)000 2 E 608 3 5 DOS 8 1 00 2 6 18 (1) 005 1 8 500 8 5 00 5 8 1 00 0 T ME 300 81 009 Ei 00001 00 Z L 00++ 000 Z - 7-NE 2N 6000 14 400 23 000 3 1000 (1) ZH-7, 5 600 4 800 7 800 1 1000 1 5000 2 2 200 (1) 0000 + 0006 5 00881 0092 HZ 0981002+10090100+L009+0002007-M 00967 007+7 0096 1 000+1 000 6 00+ CE 1741 (1)0089200761009010005 (1)0000+0008 S 000 L ( 000 Z מלכות באינה מכינה באינה באינה מלכות (מ" מ) (מ" מ) (מ" מ) (מ" מ) (מ" מ) (מ" מ) (מ" מ) (מ" מ) מבסיר מבס אורים) במלכחה במ (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) (1-11) 000 1111 000'06 000'54 000'09 000'57 000'08 000'54 000'111 000'06 000'SL 000'09 000'SD 000'08 THE WIRESHALL 5 000'06 000'51 000'09 000'59 000'08 000'5, R (zNI/z) SSBBLS BISNBL (zNI/#) 553BIG -7115(13<u>[</u> (\*NI/#) SSBAIS BILLING) (2/11/x) SS3315 3715173] TUROUED FROM MUT TOROURD FROM HEAD TUR MOST OSUDSOT TORQUED FROM HERO WAD 0314213807 OBLY NON DENOTE TENSILE STRESS REPIENED 1221-1 - AN 310 C 20 MFD BY FLEXLOR DIN OF 5TD PRESSED STEEL CO. JENKINTOWN, PA SISBHUNDAY IN FEBRUARIE FOCKWELL T. SCALE GO) CONTRACT Nº AF 33(66) 2808 SCREW OR BOLT-AN LOC-GG MED, BY HERD BOLT & SCREW CO., STAMFORD, COMM. 77/5 H1H0 1531 48-INU 11-5/1, M-M---COUNTERSINK IN HARDENED QS-HOISSEMHOS SKETCH SHOWING HERD 1585 CELL - NO.

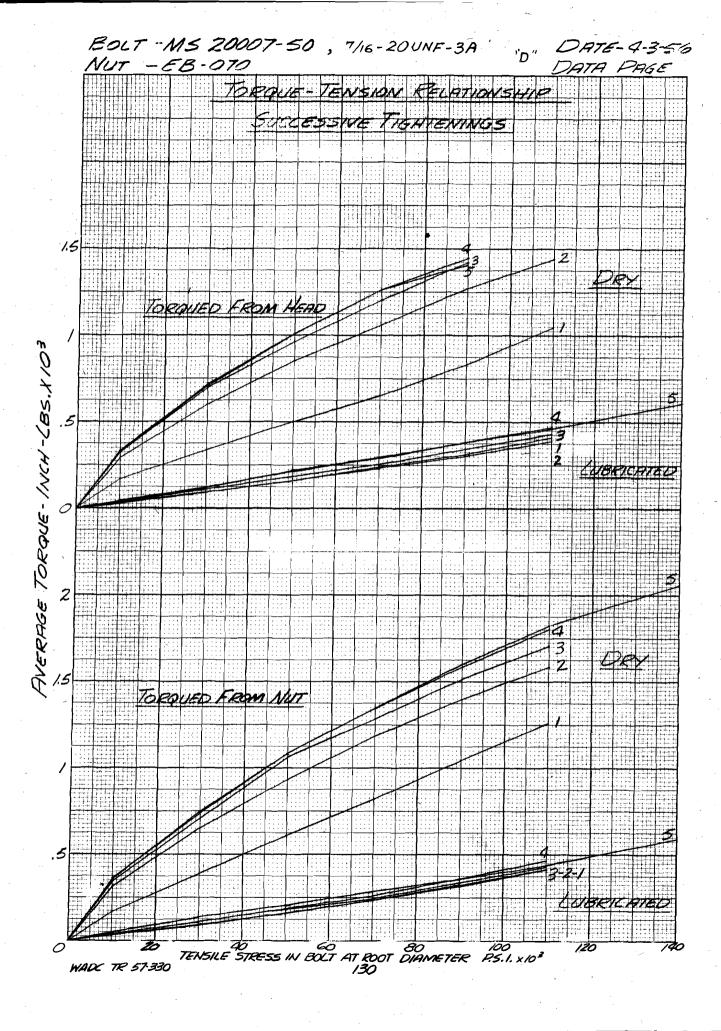
## APPENDIX IV

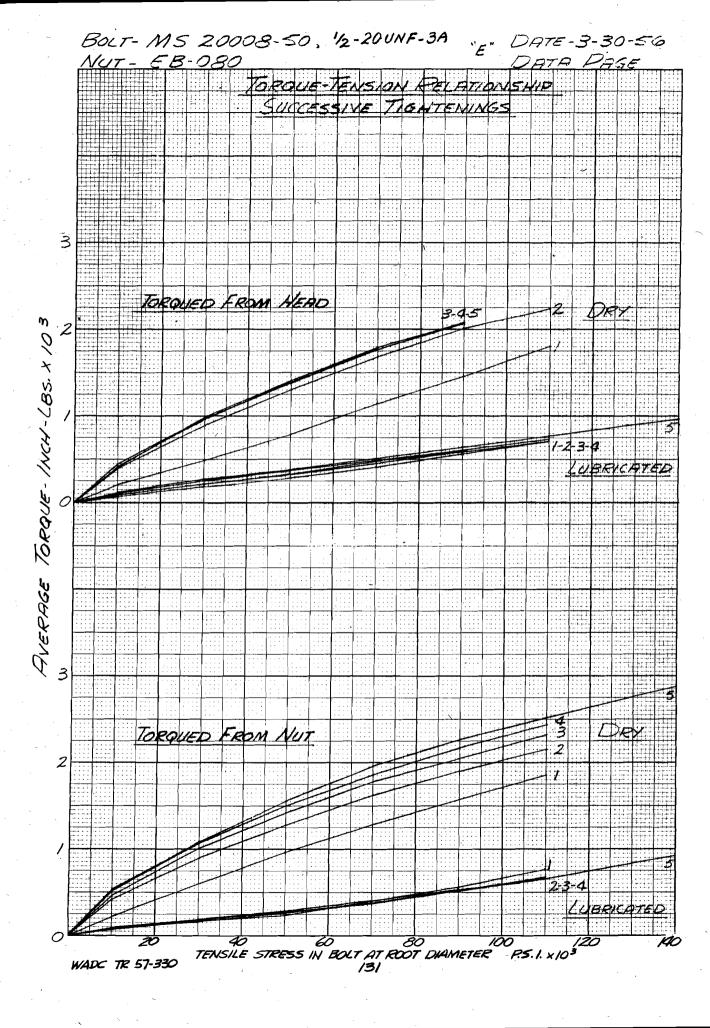
GRAPHS of TORQUE TENSION RELATIONSHIPS

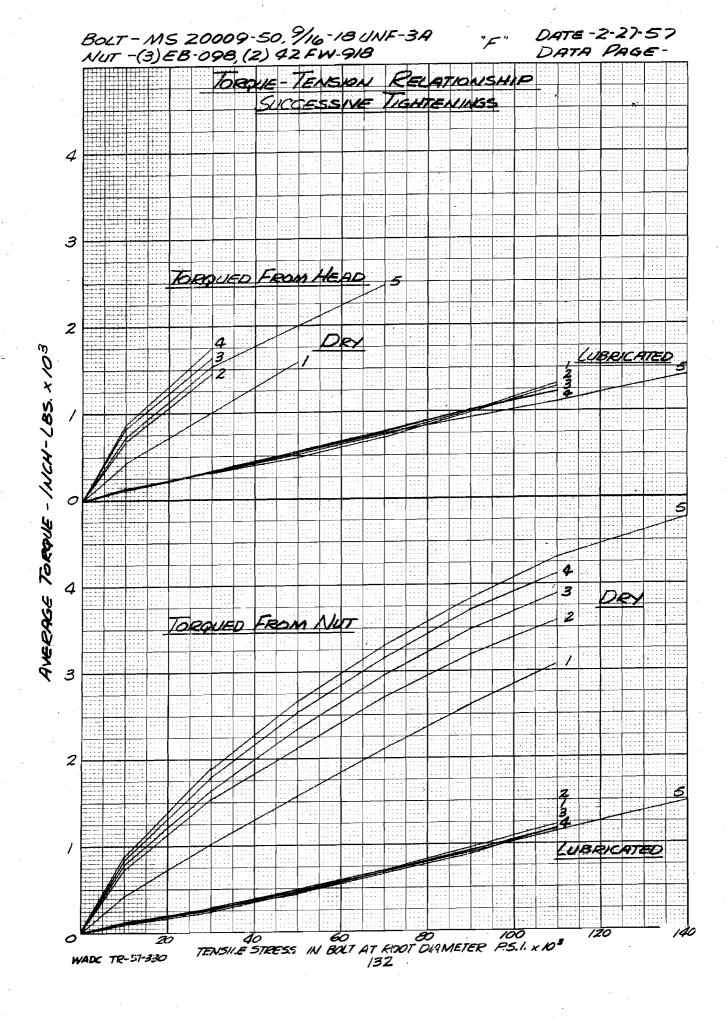


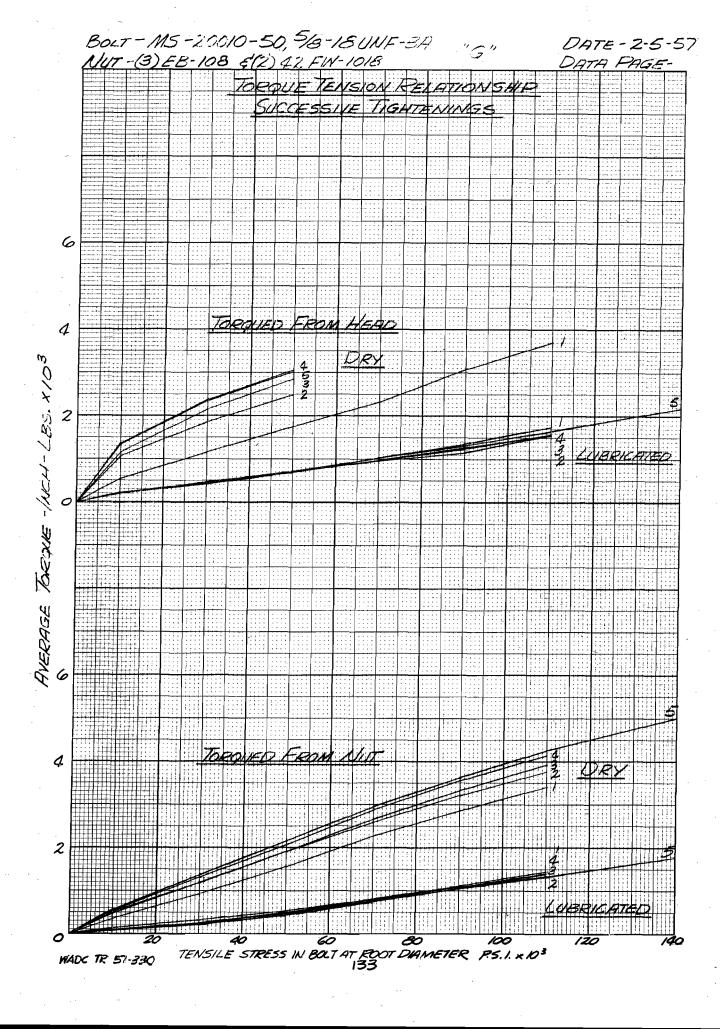


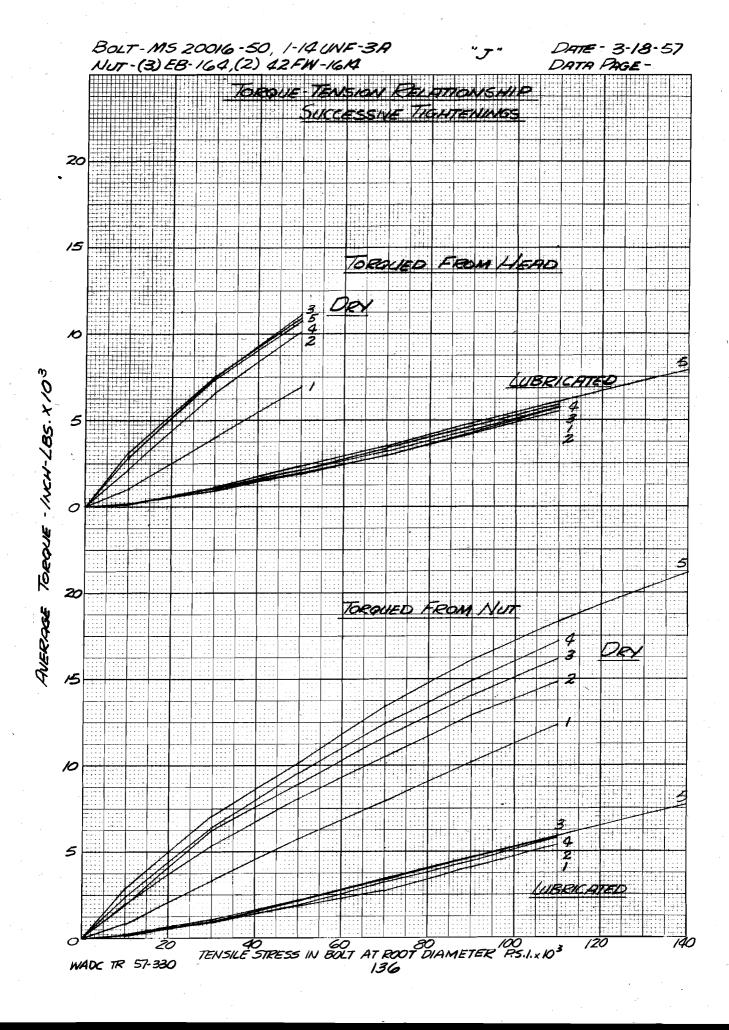


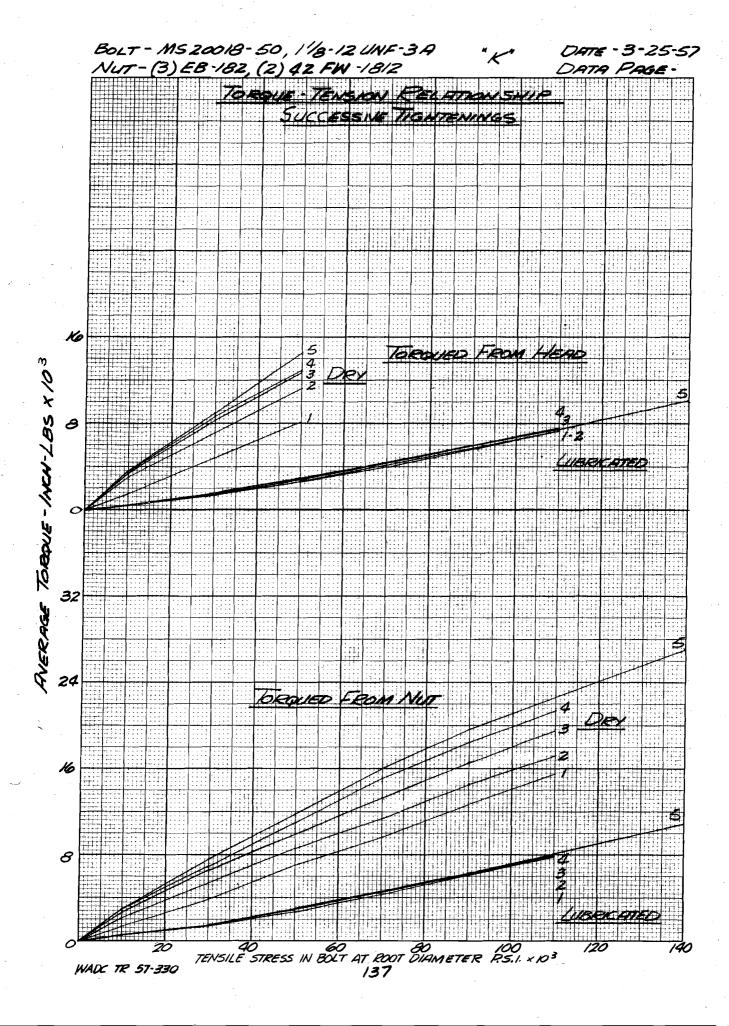


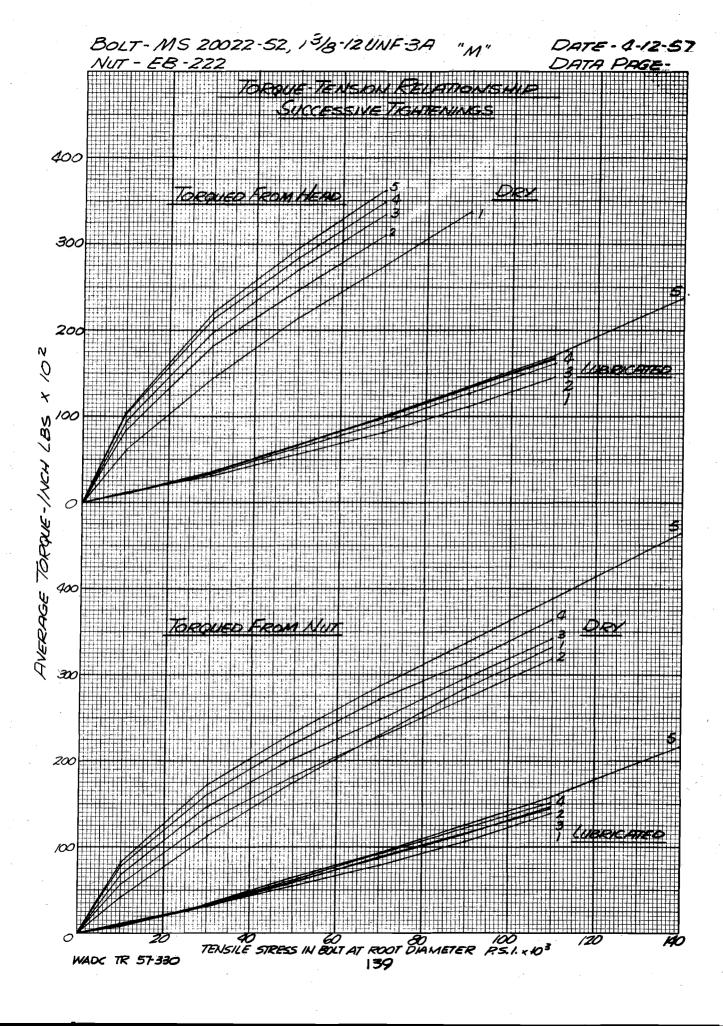


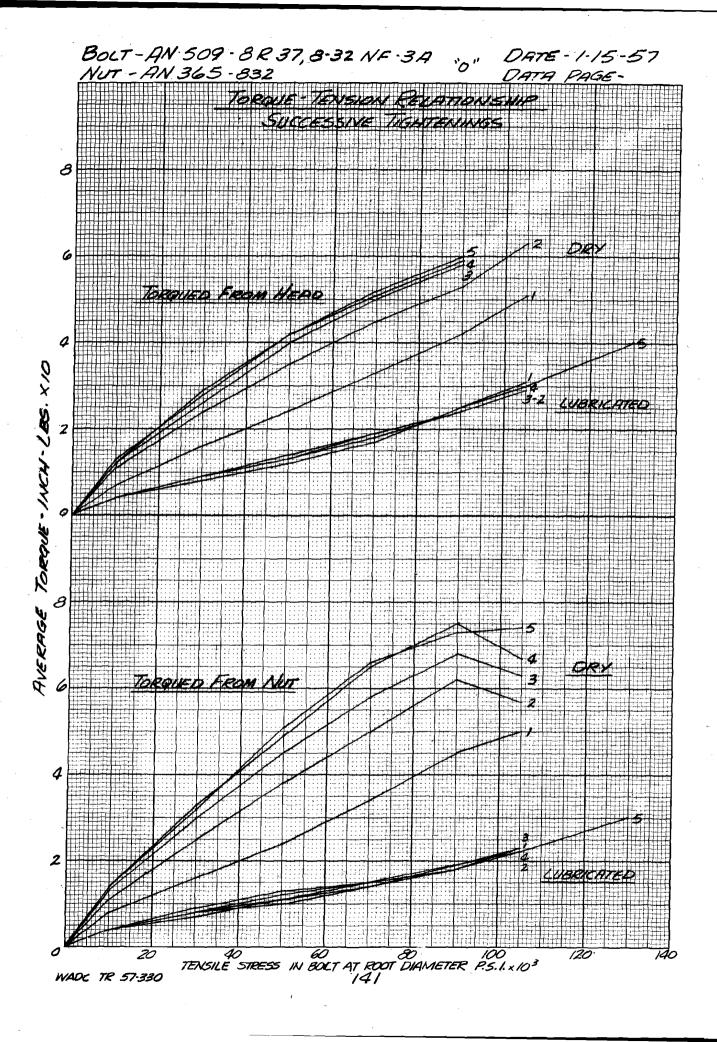


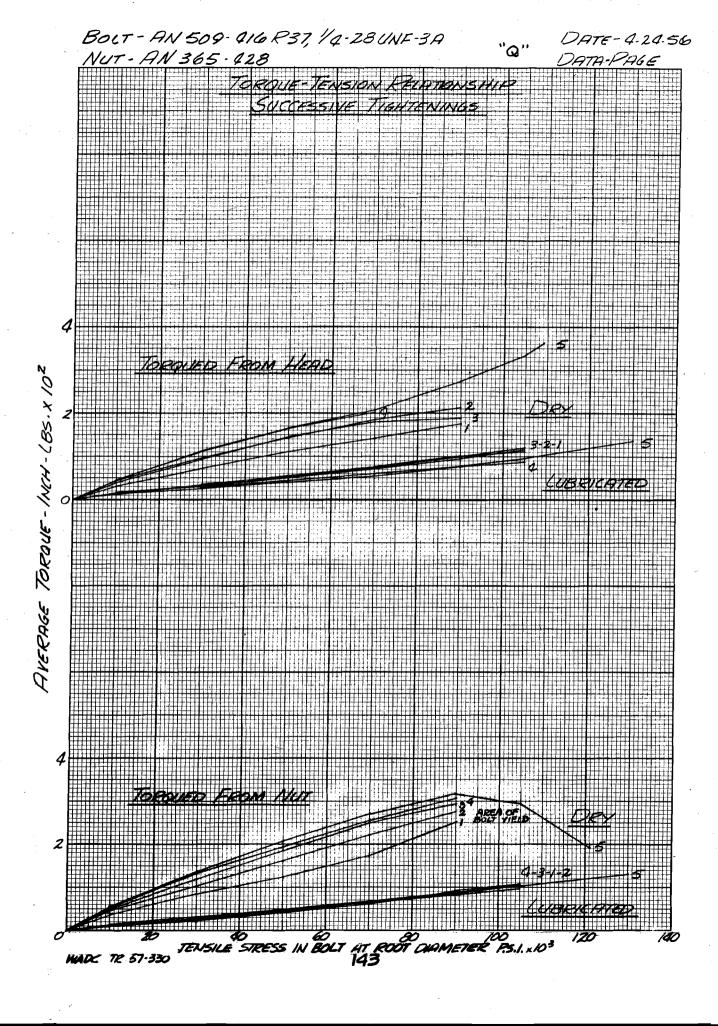


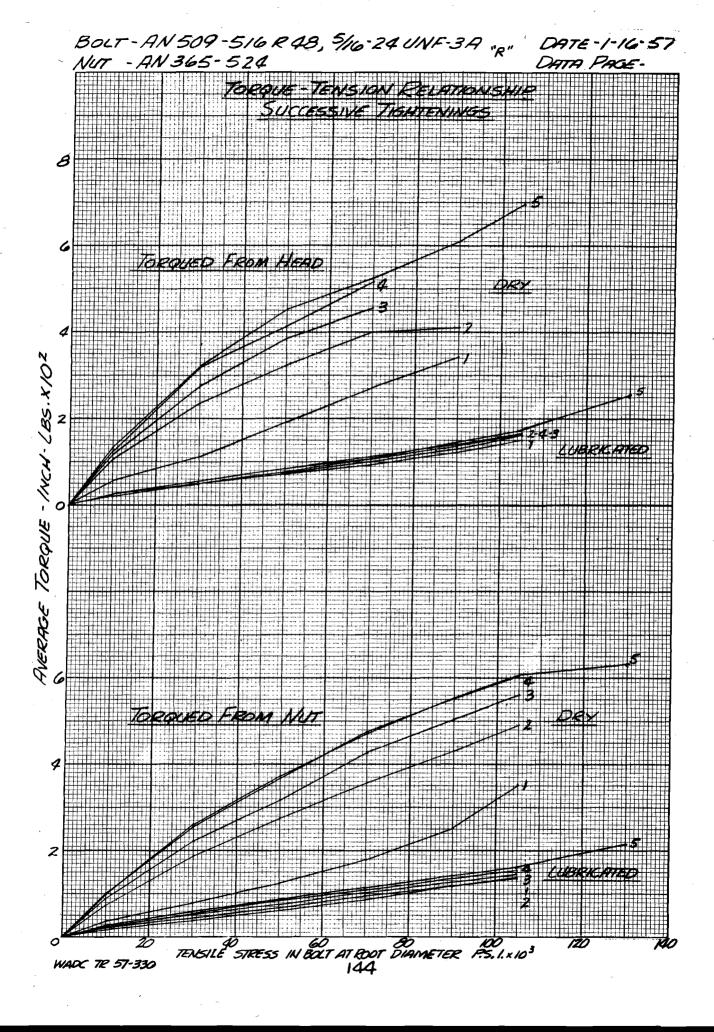


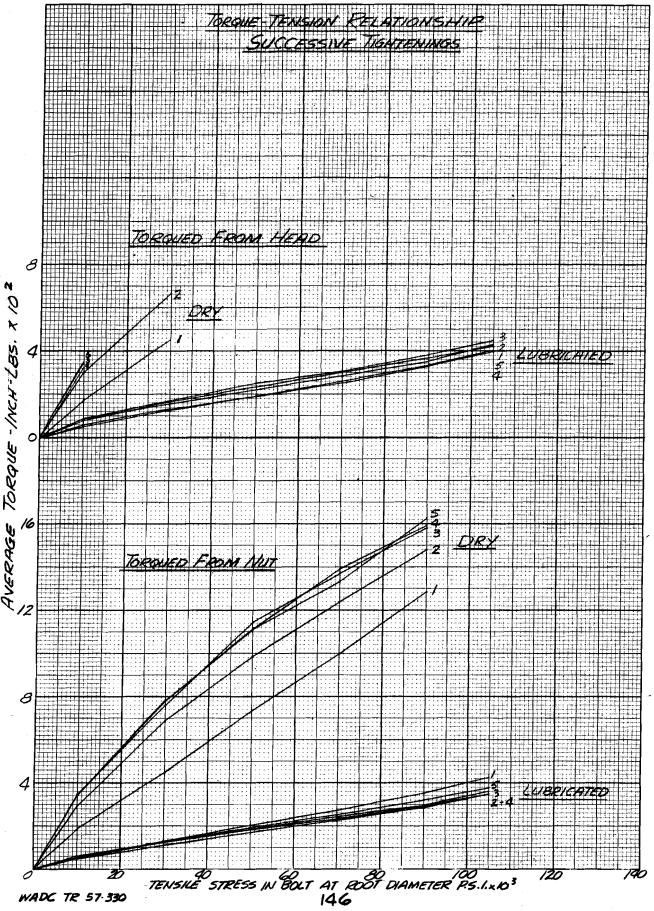


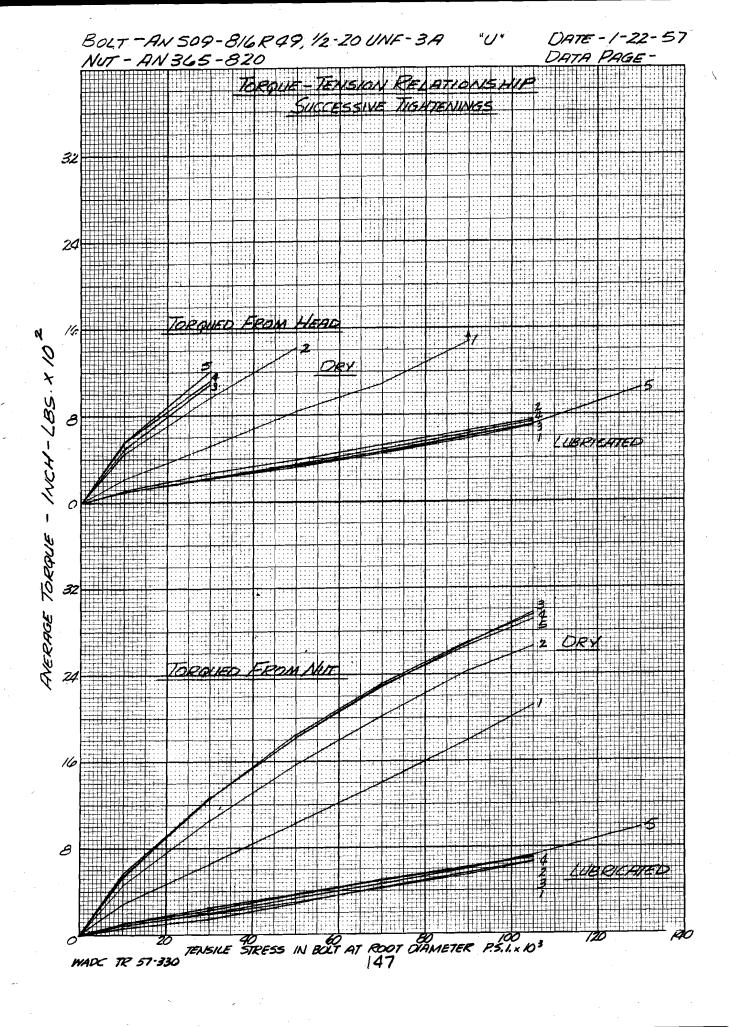


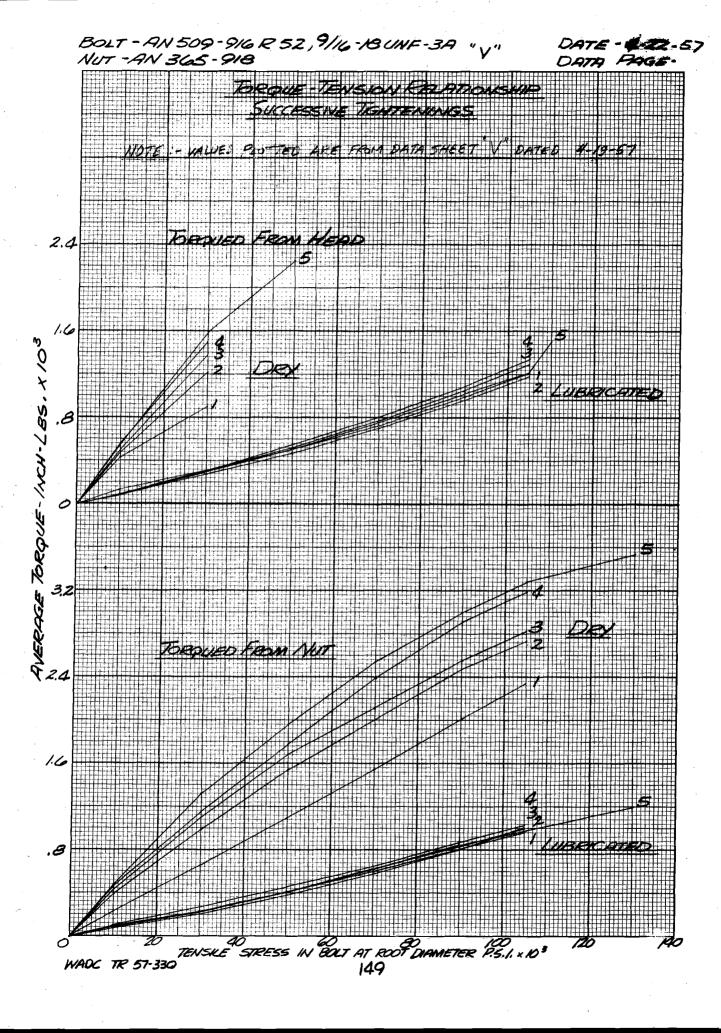


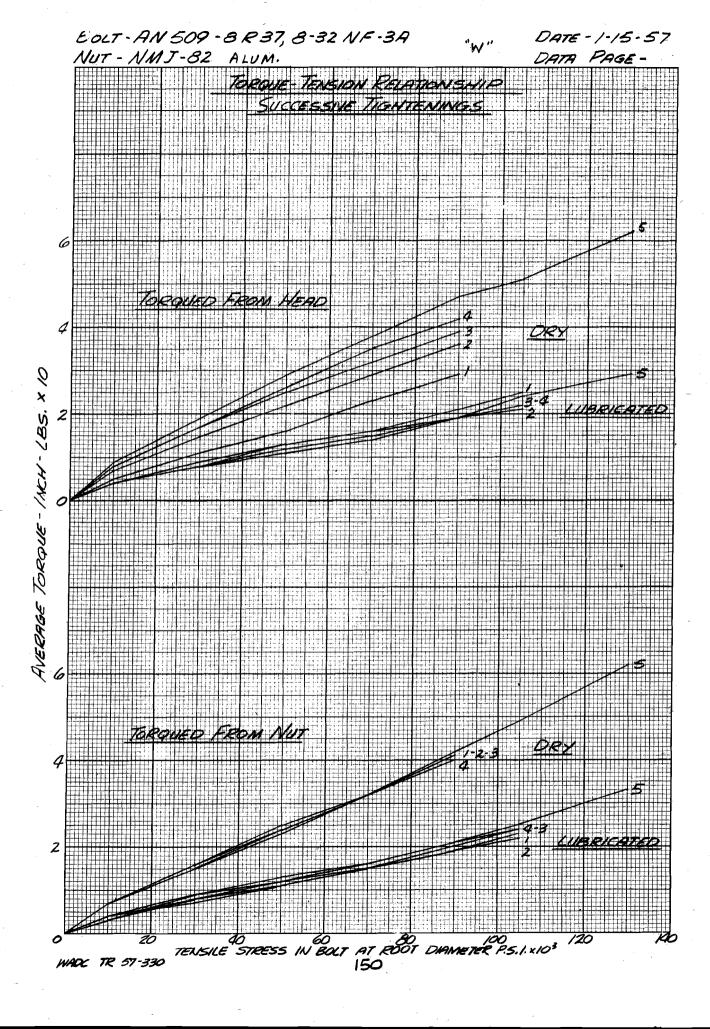












TENSILE STRESS IN BOLT AT ROOT DIAMETER P.S.I.x 103

WADC TR 57-330

WADC TR 57-330

